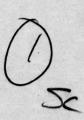




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WELDING ENGINEERING REPORT 0161

ALUMINUM WIRE SPRAY METALLIZING SHIPBOARD COMPONENTS FOR CORROSION RESISTANCE, USS William H. Standley CG-32

1 8 JUL 1978

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color code for chrome molybdenum valve body

55------Completed valves ready for transport to ship

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nozzles masked from spray to accomodate

welding. Bubbling of sealer was caused by

high welding heat input. Lower heat inputs

alleviated this condition.

59,60,61,62,63,64,65----Installed valves and components

66-----Non metallized new valve installed approximately one month before photograph. Note

corrosion spots already forming

- 1. Puget Sound Naval Shippard was tasked by COMNAVSEASYCOM to develop a procedure, qualify personnel, and aluminum spray metallize as many valves and selected other parts as practical in the main propulsion system of the USS William H. Standley CG-32. A total of 571 valves, 15 safety valve caps, eight boiler access doors, and eight small pipe assemblies were sprayed during the course of this research and development project. The project was undertaken to provide a documented, representative test of sprayed aluminum as a corrosion control method.
- 2. Two meetings were conducted at PSNS on 23 and 24 March 1978 to discuss the merits and feasability of metallizing Standley valves on a not to interfere with production basis. The meetings were attended by approximately twenty people representing shops 926, 931, 956, 938, 971; Codes 138, 213, 231, 332, 385; USS Standley; NAEC; SURFPAC; NAVSEC; and NSRDC. The consensus was that PSNS could spray the valves in a timely manner and obtain sufficient data required for this research and development project.
- 3. Welding procedure #0159 and its addendum (enclosure 1) were written to accomplish personnel qualification, provide instructions for metallizing the production valves, and provide quality assurance requirements. The welding procedure was reviewed and concurred in by representatives of SURFPAC (Bob Sulit), NSRDC (Vincent Schaper), NAEC (Mike Bless), and NAVSEC (Frank Vapniarek).
- 4. The production spraying of the valves presented some problems that were overcome and the following recommendations are presented: included.

- The small valves, &" thru 2", were completely disassembled prior to cleaning and grit blasting. New valves that were protected with cosmoline were very difficult to thoroughly vapor degrease unless all of the parts were disassembled. When the project was nearly completed, a less time consuming method was initiated. This method consisted of baking the entire assembled valve at approximately 600°F to remove the grease. Then a cotton plug was inserted into the inlet and outlet over which a rubber stopper was inserted. The stem was masked using a rubber hose pushed down into soft RTV silicone rubber that had been placed in the packing gland. After about 24 hours, the RTV was sufficiently set up to allow blasting. Preliminary blasting with send or slag removed solidified grease residue and other contaminents and then aluminum oxide blasting established the anchor pattern on the final blast.
- (b) The best material found for masking the valve internals for protection from sandblasting is the standard rubber laboratory stopper. The cotton plug under the rubber stopper insured protection of valve internals from foreign material.
- (c) Stud threads may be sprayed provided no more than three threads protrude through the nut, or the fit of nut to stud is reasonably loose.
- (d) The production line for metallizing should be in one concentrated area and consist of spaces for disassembly/reassembly, masking, vapor degreesing, baking, grit blasting, metallizing and sealing.
- (e) Oil seepage from pores in the casting or from bearing/faying surfaces has been the only cause for any non-bonding of the spray. This condition occurred on thirty-nine of the 571 valves sprayed as indicated by the "reject" indication in the spraying log (enclosure 2). Partial correction of this condition was accomplished by completely disassembling the smaller valves, vapor degreasing the parts and reassembling degreased parts for the grit blasting cycle. Later in the project, baking and improved masking techniques alleviated this problem. Where oil seeped from casting porosity in one of the large reworked valve bodies, successful spraying was accomplished after baking the valve body at 500°F, blasting off unbonded spray and respraying.
- (f) Valve identification was maintained with the use of material delivery records, stamped numbers on body/bonnet flange as shown in Fig 54, and a round metal tag with FAS stamped on it and securely fastened to the part as shown in Fig 62.

- (g) Application of the sealer on all of the valves was by brush. Spraying the sealer would be better if a work area is set up for spray painting.
- 5. The materials used during the project were frequently checked and the following observations were made:
 - (a) The aluminum oxide grit used for final blasting should not contain more than 25% fines (able to pass through a #50 sieve).
 - (b) The air used for spraying should have a dew point of +15°F or less to assure relatively dry air for spraying.
 - (c) The final blast and spraying air should not contain more than .04 ppm oil vapor.
 - (d) The aluminum wire used was chemically analyzed and was found to be 99 plus percent pure aluminum (lab report #0800 of 4/7/78).
- 6. Qualification, tensile, bend and micro tests for the metallizing operators and in-process bend tests were conducted per the requirements of the spraying procedure. Five tensile specimens and one bend specimen were sprayed by each operator. The tensile specimens were one inch diameter 4130 material and sprayed with aluminum to a thickness of .010 to .026 inch. The sprayed surfaces of the tensile specimens were then trued by sanding, lightly sandblasted and bonded to un-sprayed specimens using 3M EC2186 epoxy adhesive. After the bonding cycle was complete the assembly was pulled to obtain tensile strength of the bond line between the spray and the substrate. The average tensile of 30 specimens was 6279 psi with the low being 1600 psi and the high at 11,100 psi. Only three tensiles of the 30 were below 3000 psi and no two came from the same operator. Figure 1 thru 6 shows the sprayed ends of the specimens after separation. The bend specimens exhibited very favorable results during severe bending. The aluminum spray ranged from .004 to .011 inch on the .050 inch think carbon steel bend test strips. After spraying, the samples were subjected to a 180° bend around a k inch radius with the spray being in tension. Approximately 50% of the forty samples had minor hairline cracking in the bend, three samples failed because of excessive cracking or flaking and the rest of the specimens were essentially free of coating discontinuities. Figures 7 and 8 are representative examples of the bend specimens. Microphotographs of the cross sectioned aluminum spray are depicted in Figures 9 thru 12. The micrographs indicate the anchor pattern, density and thickness of the spray. The cross sections were taken across the approximate middle of the three inch long bend specimen. Operator training was conducted on the job after oral indoctrination by Shop 926 supervision and Code 138. Spraying proficiency became apparent after about five valve bodies were completed.
- 7. All valves sprayed during this project were closely quality controlled during the entire cycle as shown in the spraying log (enclosure 2). Also a

process operation sheet was initiated for each sprayed item. The original of this sheet ultimately remains with ships force so future monitoring can be logged. An example of a completed process operation sheet is included with the addendum to the welding procedure in this report (enclosure 1). Figures 13 and 14 indicate the flow of production spraying. The sprayed valves will be monitored for the next six years by DTNSRDC for corrosion protection effectiveness of the aluminum spray.

- 8. The following ten one half inch carbon steel globe valves were chosen to collect data on an alternate stud material; class 422, 12% chrome, corrosion resisting steel of MIL-S-861:
 - (a) Auxiliary exhaust low point drain inlet valve, lower level, STBD, Fr 128, 20 feet from CL, aft fire room, subject to 15 psi, 450°F.
 - (b) Auxiliary exhaust low point drain valve (outlet from orifice), lower level, STBD, Fr 128, 20 feet from CL, aft fire room, subject to approximately 15 psi, 450°F.
 - (c) Auxiliary exhaust low point drain valve (stop check from orifice), lower level, STBD, Fr 128, 20 feet from CL, aft fire room, subject to 15 psi, 450°F.
 - (d) Auxiliary exhaust low point drain (inlet to orifice), lower level, lower case, Fr 136, 15 feet from CL, aft fire room, subject to approximately 15 psi, 450°F.
 - (a) Auxiliary exhaust low point drain valve (outlet from orifice), lower level, lower case, Fr 136, 15 feet from CL, aft fire room, subject to approximately 15 psi, 450°F.
 - (f) Number 2A main feed pump turbine casing drain valve (outlet from orifice), upper level, port, Fr 120, 20 feet from CL, aft fire room, subject to approximately 25 psi, 450°F.
 - (g) Number 2A main feed pump turbine casing drain valve (stop check after orifice), upper level, port, Fr 120, 20 feet from CL, aft fire room, subject to approximately 25 psi, 450°F.
 - (h) Number 2B main feed pump turbine casing drain valve (outlet from orifice), upper level, port, Fr 124, 12 feet from CL, aft fire room, subject to approximately 25 psi, 450°F.
- (i) Number 2C main feed pump casing drain valve (outlet from orifice), upper level, port, Fr 124, 20 feet from CL, aft fire room, subject to approximately 25 psi, 450°F.
- (j) Number 2C main feed pump casing drain valve (stop check after orifice), upper level, port, Fr 124, 20 feet from CL, aft fire room, subject to approximately 25 psi, 450°F.

- 9. A limited number of heat treated steel studs and nuts were also "Cermatil" coated and their installation locations will be addressed on the process operation sheet for the subject valve. "Cermatil" is a type of ceramic that will withstand thread pressure and corrosive conditions.
- 10. Manpower and material cost data will be supplied by PSNS planning codes and is not addressed in this report.
- 11. Figures 15 thru 66 depict the various stages of the spraying project.

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7/18/78

Reviewed:

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CORROSION CONTROL OF VALVE BODIES BY METALLIZING

- 1. This procedure meets the requirements of NAVSEA 0919-LP-008-8010, Corrosion Control for Shipboard Launch and Recovery Systems, and shall be followed precisely when metallizing the valve bodies described in paragraph 2.
- 2. This procedure is applicable to the propulsion system valve bodies on the CG 32. USS STANDLEY.
- 3. Condition of Surface. In utilizing the wire spray method for the corrosion control of valves, a great deal of importance must be placed on the condition of the surface to which they are applied. A coating system is only as good as the care that was taken in its application, and the greatest portion of application time and effort should be devoted to surface preparation. It has been estimated that 90% of all coating failures can be attributed to poor surface preparation.
- 4. Cleaning the Surface. The application of a coating over a corroded surface should never be attempted. The corrosion products destroy the bond between the coating and the base metal. In addition, any moisture that is present in the corrosion product, no matter how minute, will cause further corrosion of the metal, and blistering of the coating will occur. The metal surface, often called the substrate, shall also be free from contaminants such as grease and oil. Even fingerprints can cause coating failures because even the smallest amount of oil present on the hand is enough to prevent a bond of the coating to the substrate. Prepared surfaces shall be handled with clean gloves or rags. A good clean surface preparation should accomplish two things:
- a. Remove all corrosion products and contaminants so that the coating can be applied on bare, clean metal.
- b. Provide a roughened surface, often called an anchor pattern, for a good mechanical bond between the coating and the metal. By far, the best means of obtaining such a surface is by abrasive (grit) blasting.
- 5. <u>Preparation for Blast</u>. All oil and grease contamination must be removed prior to the commencement of blasting. Chemically clean parts using trichlorethane, Type I, 0-T-620C.
- 6. Depending upon the type of abrasive blaster used, the blast material may be discarded after use or reclaimed. Blasting materials which have been used to remove scale shall not be used for the final blast. The reclamation process consists of cleaning and sifting the usable grit from the scale, dirt and damaged grit. NEVER REUSE GRIT WHICH HAS BEEN USED TO BLAST A VERY GREASY SURFACE. The contamination introduced in either case can be very detrimental to the coating applied over the blasted surface.

- 7. <u>Material</u>. Angular chilled iron grit or aluminum oxide grit may be used in force-feed, pressure-type blast machines.
- 8. Condition of Grit. The angular chilled iron grit will be clean and reasonably sharp. Old grit which is rusty, noticeably worn or dull when compared with new grit shall not be used. Grit having a mesh size of S.A.E. G-25 to G-40 shall be used. An individual size or a mixture may be used. The aluminum oxide grit shall be clean, sharp and free of excessive fines and shall have a mesh size of 20 to 50.
- 9. <u>Blasting Equipment</u>. The blasting equipment used shall be of the conventional force-feed pressure type. Nozzle size shall be such that a pressure of not less than 75 PSI (5.27 kgf/sq. cm) is maintained at the blast generator.
- 10. Surface Blasting. All surfaces to be flame sprayed shall be thoroughly cleaned and roughened by blasting with an abrasive described in paragraph 8. If paint, oil or bituminous materials are present, they must be removed by flame cleaning or by blast cleaning prior to the final blast operation. The abrasive used for cleaning heavily contaminated surfaces shall not be reused for the final blast, even though the abrasive is rescreened. The abrasive shall be checked periodically to see that it conforms to the requirements of paragraph 8.
- 11. Air Supply. The air supply must be sufficiently free of oil and moisture so that no visible oil or moisture appears on the blasted surface. The air supply must be adequate to maintain 75 PSI (5.27 kgf/sq. cm) minimum at the blast generator for the abrasives described above.
- 12. <u>Blasted Surface Inspection</u>. The blasted surfaces shall be inspected and approved as suitable for flame spraying before moving or dismantling the blast equipment. A sample steel plate shall be blasted until the surface cannot be further cleaned or roughened. This should be used for comparison, and any areas which do not compare favorably with the plate as to roughness or cleanliness should be reblasted.
- 13. <u>Spraying Material</u>. The wire shall be 1/8" (3.2 mm) or 3/16" (4.8 mm) diameter, METCO Aluminum, 99.0% purity.
- 14. Equipment. Any METCO wire-type flame spray gun shall be used. Use parameters shown in Appendix 1 for use with the 10E wire gun (METCO).
- 15. <u>Type of Air</u>. Clean, dry air shall be used with not less than 65 PSI air pressure. There shall not be more than 35 feet (11mm) of 3/8" ID (9.5 mm) hose between the Air Control Unit and the gun.
- 16. <u>Surface Moisture</u>. Any surface which shows visible moisture, rust, scale or other contamination shall be reblasted before spraying. The surface must be completely coated to the specified thickness within two hours of blasting. Preheat valve body to approximately 200°F. to remove moisture and control thermal expansion of body when spraying.

- 17. <u>Coating Thickness</u>. The metal coating shall be applied to a minimum thickness of .0045" (.11 mm) and a maximum thickness of .008".
- 18. <u>Number of Applications</u>. The specified thickness of coating shall be applied in multiple layers, and in no case, shall less than two passes of the flame spray gun be made over every part of the surface. The sprayed metal shall overlap on each pass of the gun to assure uniform coverage.
- 19. <u>Surface After Spraying</u>. The coating shall be firmly adherent. The surface after spraying shall be uniform and free of lumps, loosely adherent spattered metal and uncoated spots.
- 20. <u>Inspection of Metal Coating</u>. The metal coating shall be inspected for thickness by means of an approved Magnetic Thickness Gage (METCO Elecometer or equal). Inspection shall follow as closely as possible after the completion of spraying. Six as-sprayed thickness measurements and six as-sealed thickness measurements shall be taken and recorded as shown in Appendix 2.
- 21. Rejected Articles. Articles which have been rejected shall have the defective sections blasted clean of all sprayed metal prior to respraying.
- 22. Records. A Process Operation Sheet (Appendix 2) shall be completed for each valve body, and the original retained by the ship.
- 23. Finish Coating Material. The finish coating shall be METCOSEAL SA Silicone Aluminum sealer, thinned with one part METCOSEAL ST-1 Thinner to three parts sealer for spray application, or used directly from the container for brush application. Finish coatings must be applied to clean, dry flame-sprayed surfaces. Any oil, grease or other contamination should be removed by thorough washing with METCOSEAL ST Thinner until no visible traces exist. The surfaces should be allowed to dry for at least 15 minutes before applying METCOSEAL. Coatings must be applied heavily enough to produce a thoroughly wet appearance. These coatings may be applied by brush or spray.

<u>First Coat</u>. The first coat shall be METCOSEAL SA mixed as directed on container. Minimum drying time shall be 30 minutes.

Second Coat. The second coat shall be METCOSEAL SA mixed as directed on container. Minimum drying time shall be at least two hours before placing parts in service.

24. Quality Control. Metallizing operators shall be qualified by successfully metallizing five tensile specimens and one bend/micro/visual specimen. In-process quality will be monitored by requiring each operator to successfully spray at least one bend/micro/visual specimen during each shift of production spraying.

3

Prepared By 3/21/78

Approved By: Frank B. Sallo Head, Welding Engineering Div.

Encl 1

400

VARIOUS 30-40

1-2

APPENDIX 1 TO V	THE PRODUCT OF	The state of the state of			,
WIRE SPRAY PROCESS	COAT	FIHISH	FUSING PARAMETERS	BOND	COAT
BASE MATERIAL - TYPE/GRADE	crafe-Mo		FUEL GAS PSI		
PREPARATION METHOD	CHOMENTY CAR BLAST		OXYGEN PS1		
GRIT TYPE AND SIZE	CHILLED INDA	gue no	TORCH TIP TYPE		
BLAST NOTTLE TO WORK DISTANCE	4"to 6"		TORCH TIP SIZE		1
BLAST NOZZLE TO WORK ANGLE	900		FLAME TYPE REDUCING/NEAUTRAL		
GUN TYPE/MODEL	METCO		SURFACE SPEED OF PART FPM	To the R	
NOTILE TYPE AND SIZE	3/4"	3301			
FUEL GAS	ACETYLENE				
AIR CAP TYPE	EA				
FUEL GAS REGULATOR PSI	15	12 96	enegral (1886) to the	105	
OXYGEN REGULATOR PSI	40				
AIR REGULATOR PSI	72		SEALING		
FUEL GAS FLOWMETER CFH	48		TYPE OF SEALING MATERIAL USED		
OXYGEN FLOWMETER CFH	18	100			
AIR FLOWMETER CFH	36	10 19	21.7 ye72b(b - 570 - 1-25 - 74)		
WIRE TIP LENGTH - INCHES		2 10			1
WIRE SIZE / TYPE	3/16"	an take	MACHINING	10.75	
COATING TYPE	99 % PURITY		TYPE OF FINISH MACHINE		
GUN TO WORK DISTANCE	8"		FINAL MACHINING SHALL BE ACCOMP	LISHED PE	R
GUN ANGLE	900		APPROVED TECHNIQUES FOR MACHINII SPRAYED CONTINGS	NG THERMA	L
PREHEAT TEMPERATURE *F	200		(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)		
A SERVICE AND A					

NOTES: I. FUEL COXYGEN PRESSURES ARE FOR AND SPRAYING, ADJUST TO OBTAIN THE FLOWS LISTED FOR THE FLOWMETERS, IF FINAL PRESSURE IS ABOVE OR BELOW LIGHTANG PRESSURE BY MORE THAN 5 PSI AT THE FUEL GAS OR DIYGEN REGULATOR, SHUT-

MAX. TEMPERATURE OF PART OF ROTATION SPEED OF PART RPM

SURFACE SPEED OF PART FPM

TRAVERSE RATE INCHES/SECOND

E. USE METED SPRAYING TABLE & NOTES FOR FURTHER INFORMATION.

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APPENDIX 1 TO WELDING ENGINEERING PROCEDURE POIS9

THE PARAMETERS LISTED IN THIS APPENDIX SHALL BE FOLLOWED EXACTLY TO PRODUCE SATISFACTORY COATINGS FOR THE FOLLOWING USE:

POWDER FLAME SPRAY PROCESS	COAT	COAT	PLASMA FLAME SPRAY PROCESS	COAT	COAT
BASE MATERIAL - TYPE/GRADE	TOTAL ST. S.	THE PERSON	BASE MATERIAL - TYPE/GRADE		1
PREPARATION METHOD		1	PREPARATION METHOD		
GRIT TYPE AND SIZE			GRIT TYPE AND SIZE		
BLAST NOZZLE TO WORK DISTANCE			BLAST NOZZLE TO WORK DISTANCE		
BLAST NOZZLE TO WORK ANGLE		1	BLAST NOZZLE TO WORK ANGLE	-	-
GUN TYPE/MODEL			GUN TYPE/MODEL		
NOTTLE TYPE			NOTTLE TYPE AND SIZE - ANODE		
FUEL GAS TYPE		,	HOZZLE TYPE AND SIZE - CATHODE		
METERING VALVE SIZE			PRIMARY GAS TYPE		-
VIBRATOR - OFF/ON			SECONDARY GAS TYPE - CARRIER GAS		
FUEL GAS PSI			POWDER PORT - YES/NO		
OXYGEN PSI		-	POWDER ADAPTER - YES/NO		
AIR PSI			PRIMARY GAS PSI		
FUEL GAS FLOWMETER CFH			SECONDARY GAS PS1		
OXYGEN FLOWMETER CI'H			PRIMARY CONSOLE GAGE PSI		
PS AIR, JET CONVERGENCE, INCHES			SECONDARY CONSOLE GAGE PS1		
PS AIR JET PRESSURE			PRIMARY CONSOLE FLOW CFH		
FLOWMETER CONTROL VALVE SETTING			SECONDARY CONSOLE FLOW CFH		
COATING TYPE			OPEN CIRCUIT VOLTAGE DC		
GUN TO WORK DISTANCE			OPERATING VOLTAGE DC		
GUN ANGLE			AMPERES DC		
PREHEAT TEMPERATURE "F			KILOWATTS "		
ROTATION SPEED OF PART RPM			POWDER CONTROL SETTING		
SURFACE SPEED OF PART FPM		1150	POWDER FEEDER TYPE		
TRAVERSE RATE INCHES/SECOND			POWDER CARRIER GAS TYPE		
			POWDER REGULATOR PS1		
			POWDER CONSOLE PSI		
			CARRIER GAS FLOW CFH		
			RANGE SWITCH HI/LOW		
			ORIFICE SIZE		
			METER WHEEL TYPE		
			FEED RATE METER READING		
			METER WHEEL RPM		
			VERNIER DIAL SETTING		
			PEEDER HOSE-TO-GUN		
			POWDER INJECTION PORT - FRONT		
			POWDER INJECTION PORT - REAR		
			GUN TO WORK DISTANCE		
			GUN ANGLE		
			PREHEAT TEMPERATURE "F		
			POWDER TYPE		
			ROTATION SPEED OF PART RPM		
			SURFACE SPEED OF PART FPM		
			TRAVERSE RATE INCHES/SECOND		

WIRE SPRAY PROCESS	ROND	COAT	FUSING PARAMETERS	COAT	FINISH
BASE MATERIAL - TYPE/GRADE	cre/crno		FUEL GAS PS!		
PREPARATION METHOD	CHAMICALLY CLEAN (GAIT BLAST		OXYGEN PSI		
GRIT TYPE AND SIZE ALUM DENE	20 to 50		TORCH TIP TYPE		
BLAST NOTTLE TO WORK DISTANCE	4" to 6"		TORCH TIP SIZE		
BLAST NOZZLE TO WORK ANGLE	900		FLAME TYPE REDUCING/NEAUTRAL		
GUN TYPE/MODEL	METER		SURFACE SPEED OF PART FPM		
NOTTLE TYPE AND SIZE	74 16"				
FUEL GAS	ACETYLENE				
AIR CAP TYPE	EC				
FUEL GAS REGULATOR PSI	15				
OXYGEN REGULATOR PSI	40				
AIR REGULATOR PSI	72		SEALING		
FUEL GAS FLOWMETER CFH	40		TYPE OF SCALING MATERIAL USED		
OXYGEN FLOWMETER CFH	11		METCOSEAL SA		
AIR FLOWMETER CFH	34				
WIRE TIP LENGTH - INCHES	0	-6]
WIRE SIZE	\$"		MACHINING	1	
COATING TYPE	992 PURITY		TYPE OF FINISH MACHINE		
GUN TO WORK DISTANCE	8"		FINAL MACHINING SHALL BE ACCOMP		
GUN ANGLE	900		APPROVED TECHNIQUES FOR MACHINII	NG THERMA	L

SPRAYED COATINGS

NOTES: I. FUEL & OXYGEN PRESSURES ARE FOR LIGHTING ONLY. AFTER THE GUN IS LIGHTED AND SPRAYING, ADJUST TO OBTAIN THE FLOWS LISTED FOR THE FLOW METERS. IF FINAL PRESSURE IS ABOVE OR BRIOM LIGHTING.
PRESSURE BY MORE THAN 5 PSE AT THE FURL GAS OR DEVOCH REGULATOR, BHUT DOWN AND LOOK FOR TROUBLE.

PREHEAT TEMPERATURE "F

MAX. TEMPERATURE OF PART "F ROTATION SPEED OF PART RPM

SURFACE SPEED OF PART FPM

TRAVERSE RATE INCHES/SECOND

200°

400°

VARIOUS

30-40 1-2

E. USE MATTO SPRAYING TABLE & NOTES FOR FURTHER INFORMATION

APPENDIX 1 TO WELDING PROCEDURE #0159

THE PARAMETERS LISTED IN THIS APPENDIX SHALL BE FOLLOWED EXACTLY TO PRODUCE SATISFACTORY COATINGS FOR THE FOLLOWING USE:

POWDER FLAME SPRAY PROCESS	COAT	COAT	PLASMA FLAME SPRAY PROCESS	COAT	COAT
BASE MATERIAL - TYPE/GRADE			HARE MATERIAL - TYPE/GRADE		
PREPARATION METHOD			PREPARATION METHOD		
GRIT TYPE AND SIZE			GRIT TYPE AND SIZE		
HLAST NOZZIE TO WORK DISTANCE			BLAST NOZZLE TO WORK DISTANCE		
BLAST NOZZLE TO WORK ANGLE			BLAST NOZZLE TO WORK ANGLE		
GUN TYPE/MODEL			GUN TYPE/MODEL		
NOTILE TYPE			NOZZLE TYPE AND SIZE - ANODE		
FUEL GAS TYPE		,	NOZZLE TYPE AND SIZE - CATHODE		
METERING VALVE SIZE			PRIMARY GAS TYPE		
VIBRATOR - OFF/ON			SECONDARY GAS TYPE - CARRIER GAS		
FUEL GAS PSI	3 3		POWDER PORT - YES/NO	1009	
OXYGEN PSI			POWDER ADAPTER - YES/NO		
AIR PSI			PRIMARY GAS PSI		
FUEL GAS FLOWMETER CFH			SECONDARY GAS PSI		
OXYGEN FLOWMETER CI'H			PRIMARY CONSOLE GAGE PSI		
PS AIR, JET CONVERGENCE, INCHES			SECONDARY CONSOLE GAGE PSI		
PS AIR JET PRESSURE			PRIMARY CONSOLE FLOW CFH		
FLOWMETER CONTROL VALVE SETTING			SECONDARY CONSOLE FLOW CFH		
COATING TYPE			OPEN CIRCUIT VOLTAGE DC		
GUN TO WORK DISTANCE			OPERATING VOLTAGE DC		
GUN ANGLE			AMPERES DC		
PREHEAT TEMPERATURE "F			KILOWATTS		
ROTATION SPEED OF PART RPM		2,0000	POWDER CONTROL SETTING		
SURFACE SPEED OF PART IPM	no fea	th valu	POWDER FEEDER TYPE	415	
TRAVERSE RATE INCHES SECOND			POWDER CARRIER GAS TYPE		
			POWDER REGULATOR PSI		
	1000	100000	POWDER CONSOLE PSI		
-1.686.10.752.533			CARRIER GAS FLOW CFH	THE R. L.	
			RANGE SWITCH HI/LOW		
	O1 500	Line	ORIFICE SIZE		-
0.5272504	P. Sherry	Erl. Is	METER WHEEL TYPE		
			FEED RATE METER READING		
			METER WHEEL RPM		
			VERNIER DIAL SETTING		
estala isped . The no			FEEDER HOSE-TO-GUN	100	
			POWDER INJECTION PORT - FRONT		
			POWDER INJECTION PORT - REAR		
			GUN TO WORK DISTANCE		
			GUN ANGLE		
			PREHEAT TEMPERATURE *F		
			POWDER TYPE		
			ROTATION SPEED OF PART RPM		
			SURFACE SPEED OF PART FPM		
men father (flores ands)			TRAVERSE RATE INCHES/SECOND	6 99	

ADDENDUM TO WELDING PROCEDURE 0159

PURPOSE

To specify quality control requirements for metallizing of steam system valves.

SCOPE

This addendum applies to metallizing of ship steam valves accomplished under NAVSHIPYDPUGET Welding Procedure 0159.

REQUIREMENTS

A. Visual Inspection.

- 1. Prior to abrasive blasting each valve shall be visually inspected to assure removal of grease and oil contaminants.
- 2. Each valve shall be thoroughly inspected for compliance to surface cleanliness and roughness standards prior to metallizing.
- 3. Each valve shall be inspected after metallizing to assure coated surface is uniform and free of lumps or uncoated areas.
- 4. The metallize coating shall be measured to verify that a minimum thickness of .0045 in. (.11 mm) has been attained.
- B. <u>Testing</u>. Bend/micro/visual testing shall be conducted on one test specimen from each metallizing operator per shift. Steel plates $1-1/2 \times 3$ inches, of approximately .050 inch thickness, shall be metallized and serve as the test specimen.
- C. <u>Marking</u>. Each valve shall be marked as follows to provide unique traceability to process/inspection documentation:
- 1. Letter "S" followed by the last three digits of the valve's Material Delivery Record (MDR) (Form 13ND PSNS 4840/1) serial number. These markings shall be followed by the letters "PS" and a number indicating the chronological order the valve was processed. For example, the eighth valve processed for a lot having MDR number 56-300304 would be marked S 804 PS8.
- 2. Marking shall be applied by die stamping with round-bottom, low stress die stamps. Depth of the impression shall not exceed 0.010 inch. The marking shall be applied to both flanges at the intersection of bonnet to body on the flow arrow side of the valve. These markings shall be clearly visible after metallizing.

Encl 1

D. Material Control.

- 1. Valves shall be traceable to their applicable MDR's throughout processing. Base material of new valves shall be identifiable through re-application of original color code markings after metallization.
 - 2. Grit blast material shall be periodically inspected for useability.
- E. Operator Qualifications. Prior to commencement of production flame spraying, each metallizing operator shall be qualified by successfully flame spraying five tensile and one bend test specimen. Each operator shall maintain qualifications by successfully flame spraying one bend test specimen per shift.

PROCEDURES

1. Production Department

1.1 Shop 31

- 1.1.1 Assign a number and mark each valve in accordance with Section C. of Requirements prior to valve cleaning and blasting.
- 1.1.2 Maintain a log by assigned valve number which provides a description of each valve, including the valve's MDR number. For new valves, the log shall include the valve base material and color coding. Request Shop 26 to pick up valves for delivery to Shop 71.
- 1.1.3 Upon completion of metallizing, refurbish valves as required. Assure all new valves have been color coded to match their original color code marking. Forward valves with applicable Wire Spray Process Operation Sheets (13ND PSNS 9074/1) to Shops 38, 56 or ships force as applicable for installation.

1.2 Shop 72

- 1.2.1 Prior to initial valve blasting, and weekly thereafter during production, forward a sample of the abrasive grit to Code 134.1 for sieve analysis. Request the analysis via NDT Request (Form 13ND PSNS 4730/26). Scrap all abrasive grit which fails this analysis.
- 1.2.2 Assure all incoming valves have been stamped with an assigned valve number. Log in each valve by valve number and MDR number. For color coded new valves, identify color code in log book.
- 1.2.3 Prior to abrasive blasting, visually inspect each valve to assure removal of grease and oil containments. Clean valves with Trichlorethane, Type I, 0-T-620C, as necessary to satisfy the inspection.
- 1.2.4 Protect all internal openings with rubber plugs or metal cups and mask all threads prior to grit blasting.

- 1.2.5 Following completion of blasting, handle the valves with clean gloves or rags and place them within a polyethylene bag or covering. Attach a tag indicating valve and MDR number, color code marking on valve at time of receipt if applicable, and time/date blastingwas completed. Alert Shop 26 that valves are ready for pick up.
- 1.2.6 Enter data in applicable blocks of the Wire Spray Process Operation Sheet (13ND PSNS 9074/1).

 Provide the records with the valves to Shop 26.

1.3 Shop 26

1.3.1 Initiate and enter applicable data on the Wire Spray Process Operation Sheet (13ND PSNS 9074/1) for each valve. (See enclosure (1) for example). Expedite valves and records to and from Shop 71.

NOTE: Handling of clean valves shall be accomplished with clean gloves or rags.

1.3.2 Inspect blasted surfaces for adequacy of cleanliness and roughness. Certify satisfactory surface preparation on Wire Spray Process Operation Sheet.

NOTE: Have a sample steel plate grit blasted until the surface cannot be further cleaned or roughened. Use this sample as a standard for the surface preparation inspection.

- 1.3.3 For weld end valves, mask off 1/2-inch on the weld ends of the valve before flame spraying. (This is necessary to allow for NDT of joint weld upon valve installation).
- 1.3.4 Prior to flame spraying, preheat valves to $175^{\circ}F \pm 25^{\circ}$ by use of torch or flame spray gun. Use a pyrometer to measure and control the temperature.
- 1.3.5 Assure metallizing is accomplished only by qualified operators.
- 1.3.6 Maintain a log of all valves metallized. The log shall identify each valve by assigned number and MDR number. The log shall include time of abrasive blasting completion, time of metallizing completion and time of completion of each coat of sealer. If the valve was color coded prior to cleaning/blasting (as indicated on the Shop 71 initiated tag accompanying the valve), enter the applicable color coding in the log.
- 1.3.7 Perform visual inspection of surface condition after flame spraying. Surface shall be free of lumps, spattered metal and uncoated spots. Discrepant areas must be blasted clean of all sprayed metal prior to respraying. Uncoated spots may be sprayed if the surface is completely dry and free of containination. Identify repaired areas in the "Remarks" block of the Wire Spray Process Operation Sheet. Assure metal coating was applied within two hours of grit blasting completion. Certify acceptable coating on Wire Spray Process Operation Sheet.

- 1.3.8 Use Magnetic Thickness Gage (Metco Elcometer or equal) to measure coating thickness. The measurements are to be taken in areas as specified on the back of the Wire Spray Process Operation Sheet. Assure a minimum coating of .0045 in. (.11 mm) is attained. (A coating of .005 in. (.13 mm) is desired, however, coatings exceeding this thickness are acceptable). If coating is below minimum specified, additional sprayed metal may be added if the surface is completely dry and free of contamination. When the coating meets the thickness specification, record the measurements on the Wire Spray Process Operation Sheet.
- 1.3.9 Assure first coat of aluminum sealer is allowed to dry at least thirty minutes before application of the second coat. Measure and record final finish thickness and certify completion of metallization on the Wire Spray Process Operation Sheet. Spray paint color code new valves (for material identification) to match original color coding if color coding was indicated on Shop 71 initiated tag accompaying each valve. Make a copy of each Wire Spray Process Operation Sheet and retain the copy until ship's departure. Forward valves along with Wire Spray Process Operation Sheet hardcards to Shop 31.

1.4 Shop 38 or 56 -

- 1.4.1 Install valves as applicable. If valve is nicked or gouged during transit or installation, brush METCOSEAL SA on the damaged area. METCOSEAL SA shall be mixed as directed on the container.
- 1.4.2 Enter valve installation location on applicable Wire Spray Process Operation Sheet (13ND PSNS 9074/1). (See enclosure (1) for example). Make and forward a copy of the record to Code 138. Provide Wire Spray Process Operation Sheet hardcard to the Ship's Force.
- Quality Assurance Office (Codes 134, 136, 138)
- 2.1 Analytical Chemistry Branch (Code 134.1). Perform sieve analysis of abrasive grit as requested. Acceptable iron grit shall be oil free and have a mesh size of S.A.E. G-25 to G-40. Acceptable aluminum oxide grit shall have a mesh size of 20 to 50 and be free of oil contamination.
- 2.2 <u>Metallurgy and Material Control Branch (Code 134.6)</u>. Perform physical testing of metallized test specimens as requested.
- 2.3 <u>Welding Engineering Division (Code 138)</u>
- 2.3.1 Prepare procedures for the qualification of flame spray operators to the requirements of NAVSEA 0919-LP-008-8010.
- 2.3.2 Perform bend/micro/visual analysis of operator test specimens. Request Code 134.6 assistance as necessary.
- 2.3.3 Evaluate test specimen results for adequacy of process and operator performance.

2.3.4 Provide technical information to all shops and codes concerned in regard to metallizing operations.

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2.3.5 Retain a copy of each completed Wire Spray Process Operation Sheet (13ND PSNS 9074/1) for six years.

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APPROVED: D. G. COGLIZER
Head, Welding Engineering Div.

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Enclosure (1) Sheet 2 of 2

1 OF WELDING PROLEDURE +0159

COMPLETION VERIFICATION OF OPERATION SHEET - SHOP 26 FOREMAN (Signature/date)

SPRAYED PER APPENDIX

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Encl 2

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1884 L988		CFE		10:30 7	1-4-7 Shid		11:15	7	4-7-13
1 2 3 d 2 . b b 6 9		CFE		1220 44	17:20 16	175.84	18:05	1	7.C.X
6 999-PS80.		CFE		11:20 4.6	17:20 4:02	PS 80	18:01		46.73
6890.PS 87		CFE		10:30 4.7	10145 47		11.19		4-7-7
199-1 PS 85		CFE		10.304.7	10:45 42		1	1	4-7-18
-		CFE		10:344.7	1	7 PS 83		1	4-7-78
5 244 . PS 31 . 7	Petune 115	STEEL	Remi	10:00 4.7		1250 BI-H	/3.		2-111-2
P\$ 30.	Altuens / M	STEEL	Rine	16:00 4-7					X-01-4
533	1	STEEL	0	D.W 4-6		9			4-7-78
5245 PS32 A	Attasse 1 37	3,000	Regard	16:16 47			,		4-19-7
2850		STEEL	•	14:30	1.h 36.61	7 28 95	157		4-7-19
S 554 3 PC 55	200	CAMO		10:30 42	1		11:15	4	82-2-8
Sezza estien		Clus		17.30 4.4			P. 116 1805	١	9-6.75
1 23 20 5 15 E	-2	Chino		17.36 9.6				1	31-5-4
1. 95 St. 18	-	ckmo	Soul But Little	17:30 4.4.	35.58 114	- 10 - 10 m		1	16.75
1			40	1100	21 %		_		
575.3056 A		Camo		40.50%	29. 50. 12.0.		u	300	4.6.9.4
5973.5 PS 117 .		CRAO		PO-50 4-1	19:50 4		1	1	4.4.26
1973 pe 104 V		CRMO	:	N. 30 4.6	3				1.1.7
1.911848.818		owar		1120 4-1				1	4.7.76
5925 PS 112 .		ckmo		17.30 44		46	1	1.	7.6.76
5923 8 85 113W		CRMO		11:30 4.6					36-7-6
5523 108 1106		CAMO		16:30 4.6					31-9-7
S923 2 85115 W		ckmo	•	17:30 46	17:30 4	,	`		£.6.78
59511 65 103		CRMO		17:30 4-6	1-			1	4-6-76
29732 15 94 4		CRMO		17:30H4	17.40 4-6		PS- 94 (##	6 - 4	-9.6.78
1	1	STEEL		14:00 410	14:30 4-10		PS-100 15100	1	4-10-X
41	day.	Steel		14004-7	15.45 4	4.10 B	97 17:10	1	4/10/10
PSC) 99	*	steel		14 CC 446	14:30 4	4-1C B	PS 79 1500		4.10-13
1		8.4	CRACKED		Prin 1				
1	Carpe	STECK	11.69	14:00 4-9	1	Who PSPO!	0745		8-11-3
07	76.00	Strek		6-1 00:11	15.45 4	Hie P	PX 107 16:35	-	A-10-76
* . 601	Guy .	Steck	4	1500 4-6	2130 4/2			4 -	-76
301 50	And we	Stech		1400 H-C	21. 1º "		PS 16E 22:60	.1	31:17
200 6	lung	STEEL		C-1 okio	2187			1	81.4.
5105	Cary	Street	Rycart	1400 4-12	(300 4.0	2018	5. 1400		4-13-78
1	1			1			1		
	.	- 0233		1400 49	1650 4/10		PS 130 19	19:00 47	4-10-78
50501315121	16,50	1		不作	1				1
100 SILS 331		CAMO		18:30	18:30 4-7	7 PS 35	35 1850	100	711
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		,							0 11.

Incl 2

SEVE NO.	JAIVE NO. RECIEVED	MATERIAL	LEVEL	CLCARED	-	VALVE	SPRAY TI	SPRAY TIME S
0503PS13	M. Gim	5840		11.10 4.10	16.50 X 31	1		32/ort
502.PS131	16:50	CRIME		1	18.50		35.00	11/2
5050 PS 1351	16.50	Strel	Section T	1	1000	1		1
SOSOSOSIA	25,15.50	CKUNO	Sign't -	- 1	16.00 sty		_	01-7
PILSOPPER		CROWL		14.00 H-10	21.35 4-10	Core - PS 119	21:40	420
5950-1 PS1219	,	CANO		01-1 ODE		Cern PS 121		1-10
Sosos PSIZ!	V 1650	Steek		1400 4-2	16:30 4.7	Street	_	477
Sososges	16:30	Ceno	Reject	11-10 d-16	11.50 11.11	C. Renf 3134	15:00	
DE 31 XX 21 SQ LICEOS	3	Cheric	,	1400 4-7	16.30 4.7	CROM	19:50	4/1.
S05023 PSIZ		STEEL		1400 470	0835 4.11	D21-50	510	1.1/
SOCO-1 (512.3V	34	CENE		1460 4-10	21:25 4-10	Cente - PS 1.25	-	4/10
50:20:6 85132	.25	CSADO		N.00 4.6	14:30 4-K	P5138	1500	4-10
SOSDIOPSIZA	28/	CRNO		1400 4-1C	21.25 4/10	Cenc - 25.123	21.20	+-10
2APA-S PK HOST	- Leye	STEEL		2Fh 0001	10:30 4-13	Pslles	11:00	4-13
1804-5- Pelle	,	STEEL		21-1 0001	10.50 4-15	PS 144	11:00	4-15
Acu -5-4158	9	STEEL			10:30 4-13	PS 158	11:00	4-13
404-5-PS 162	1	STEEL					13:00	4-14
88 - BEV		STEEL						
1 X		STEEL						
APR S- PSIGO	or low	STEEL		13:00 473	11:30 414	P5/40	13:00	4-14
247-5- PS 159	1	STEE			4-14 10:30 4-13	PS 159	1100	4-13
282-5-0611	1	STEF		11-10001	4-12/0:30 4-13	PSILLI	11:00	4-13
285H-1-15138	1	STEEL	1	4.12	10:30 4-13	PS136	11:00	4-13
101 -4- Pe 189	1	STEP		214	10:30413	15189	00%	4-13
PS 102	1	STELL		4-12	13:00 4-13	10300	1400	57-13
241-5-PSI	20 - Lange	STEEL		1	E1-4 0001 21-4	PS 140	11:00	4-13
92-5-PC	1	STEEL		472	1	Ì	11:00	4-13
IASH S- PE	143	STEEL		4.12	1	PS-143	11:00	4-13
82 -5- PS	142	STEEL		21-10001	4-12 1000 4-13	PSIVE	11:00	4-13
181 -5PS - 14		STEEL		1000 4-12	1000 473	PS (43	1100	4-13
Switzeling.		Shinist.		1		-		
Soug 10 PSIUT		Cama		13.30 4-11	15:30	R1+7	16:00 - 42-76	42-76
5048-IV PSIS		camo		17-1 08.5.	4-11 15:00	25152	15.45	4-11-16
3048.11 PS15		CRMG		1	4-11 21:15	PS 153	22:00:	4-11-78
SGTE & PSIUM		CRMO			4.12.21.30	PS 144	23:10 - 5	4 12.16
59662 05157		CRMO		10.30 y-11	4-11 21.15	PS 157	21:50 - 3	4-11-78
5930 .170		CRMS		13.30 4-11	111 21:15	PS/70	32:25.	82-11-4
5.048 -1 PSISH		CPMG	- Ruch	1		1	10:45	4-12:78
וווסטתרו		Chms.		92-4 6001	4-26 13:30		1	4-36-78
S050-9 PS 156		Cemo			4-11 1750	3.6	- 1	31-11-6
						-		30

YALVE NO.		MATERIAL	LEYEL	GLEANING.	BLASTINGS TIME DATE	VALVE	SPERY TIMP
6978 PS 137		CFE		-	14:30 4-11	PS 137	13:00 4-11
S0808 PS 155		CRMO			90;c/ 11-h	PS 155	15:15 4-11.78
6060 '4 PS136		CAMO		11-h 00h1	14:30 4-11	PS 136	
5049.5 PS149		CFE		1330 9-11	4-11 15:00	PS. 149	(5.50
SOURIZ PSIUS		CFE	+ Pract	11-h pa.h!	30.20	12 12 12 12 12 12 12 12 12 12 12 12 12 1	
3964318166		ckmo		13:30 4-11	4-11 17:30	PS 166	18:30
Soul 16 PSI48		CRMO		1400 410	14:30 4-11	PSI48	1500
5966. 12 169		CRMO		13:30 11-11	4-1/ 17:30	PS 149	1050 - 4
SO4 8.8 PSUS		CRMO		B:30 4-11		PS 150	000
5977.PS167		CRMO	8	B'3¢ 44		PS 147	_
5975.1 PSIL8		CRMO			4-12 21:20	PSIGB	
5018 -9 PSIST		CDMD		11-11	4-11 21:15	P\$ 151	.,
5980.3 PS174		CKMO				41150	18:00 - 4-11-7P
5C5C.10.025C		1	- Rict -	1330 4-11	4.12 (3) %	PE-175	17:00 - 4-12-78
	4			13:30 4-11	H-11 17:30	P5172	
5966. 1 PS 176		CEMB		1330 4-11	13:30 4-12	PS-176	
4		CKNID		13:30 4-11	18:00 4-12	. 281.85	-
594.4 PS178		CENTE		13:30 911	4-11 21:15	PS.178	22:40
-		CRAB		130 4-11		PS 186	
		CKMP	+ Pint		13.70 4.12.76	25, 180	11.55 4-1276
_]		CKMB		13:30 4-11	4-11 1330 4-12	PS179	14:30 4-12-7
_		CRMO	+ Court	- 1	(150 mg	85-18	\$ 20 7:50
		CEMO		1500 4-12	4-12/17.25 4-17	PS 18%	18:10 - 4:07.75
		CRATO	Defect	1	21-4 0001 11-4	PS 191	1100 4-12-78
23		CKAC		13.30 4-11	4-11 19:20	PS 183	,
4	The state of the s	CFE	The same	W:00 410 4.14		PS 182	29:10 - 4:11:75
77		CRME	* Chiet	1400 472/5:30	21-1 2:51	PS.181	16:45 -4-12-75
7		CRMO		1400 4-12/8.00	1.600 4.12	PS 173	16:30 - 4-12-78
2018 4 PS 177		5K40		13:30 4-11-100	21-6 001	23.177	1100 1-12-7
2/3		1800				PS-184	81-21-h no:11
5475. 12 187	000	CPANO		_	स्क नम	12,00	21:45 -4.12.76
PT-1P	2.0	PuPe	-	11-16	10:00 4-12	110	11:00 4-12
M-27	Diet	PiRe			1	2,40	11:00 4-12
PT-3P	=	PIPE		_	21-6 00:01	340	1
PT-4P	,	PIP		13:30 11-11	10:00 4-12	450	
PT-52	1-	MPP			10:00 4+2	975	21-6 00:11
	-	PIPP		13:30 4-11	10:00 412	610	11.00
4		CKMO		113:30 4-12 18:10	18:10 4-12	PS 201	19:10 - 4-12-78
5448.1 05195		cking 7		1	4-11 13:30 4-12	PS 195	14:30 4-12
1		CAME		1	-1	CS 190	A3:00 -4-12-75
1 5 1 4 B CC 140		000		13:30 4-11	4-11-22-4-17	30, 30	

Chite No 1		Metraink, b	Level	Times Dute	-	Tires . Dail	Ting.	Valve	Speny Ting
150 1015		E CFE		11:30	11-11	Je 30 4.12	71.4	PS: 204	4
576C.3 P. 200		CEMP		03:50	1-4	16:10	11.4	PS 200	
4974 FX 202		cre.		13.30	11.11	20:20	-4.12	PS. 202	_
Sest. 21 PS M7		CKNO	-	13:30	11.4	18:10	472	PS 197	-
5016.12 PSIY		ckmp		13:30	11.4	18:00	4-12	PS. 199	
50089 PS203		CFE	-	·	11.4	10:00	41	PS 203	
	THE PARTY OF THE P	(PMD B	41745	13.3	11-11	1400	4-18	P5196	-
	1	CENO		13:30	11-1	13:30	4-12	PSIGA	
Soc 15 PS 192		CKAB		13:30	11-6		412	PS 157	14.50 4.12
CAS.25 5 194		CKMD	-	13:30	-	21:30	4-12	46150	
Dr-7P	op.O	PIPP		13:30	11-6	1	4-12	7.0	
PT-8P	pip	PIPE		13:30	-		4-12	48	1
DS221	tot	STEEL		00.5/	4-12		4-14	PS 221	
De777	loval	STEEL	emy	0037			N-1	18237	1_
5022.9 15.2h		CRAO		15:00	417		4-17	DC 204	_
Sec. 3 Pall.		CRMC	Ment Decer	(5.00	4-12		4-12	Dr 30	-
50.29 3 15.26	Dop-9-24SES	CEAN	1	1500	4-4		11-19	Band	03.01
250 65	1	CRMO		15:00	4-12	1	4.12	Dr. 22	
COC7 PC.745		CFE		Knd	11-12		4	00. 20	
1		(640)	Or TO THE	15.00			d-1x	OF 222	10.50 4-11.A
1054 C MUZ	Pop-P-24555	CRANG	Orac T.	1500		1	4-18	Clexy	75.70 1 16 7
-		CRAD		15.00			4.18	DC 220	
		CRMO	WE 43 61 5 KB		MAZ	_	4-13	26 220	1730 - 412 7
=	POD-P-24555	CKMO	Part -	1500	11-14	2700	4-18	D 5 0 29	16261 1107
5.29 PS214		CRME	Plin	15.00	4 17	4-1: 0700 th	T,	P.S.314	AST SING
-		CRMG	-4.mc/pc	15:00	472	4-12 0830 434+	The second	PKAN	
1	*	CKAIG	-	0250	H-12	H-12 21:00 4-13	1./3	Pr 221	1
	*	CRMO	-	1500	112/	17.25 9	4-17	P. 225	18 an Jun 22
		CKAR		15:00	4-12		4-15	Deans	36 31 4 31.76
C72 FY72		C Mr		1,500	4-12		4-17	PSals	9-11-18 Die
65.36 F.E.		C/Wg		2500	472	1500 4	4-17-18	25.269	15rd -4-1-7
CZG P.C.		CRANO		1500	412	21.30 7	4.17	PS 207	22:65 4.17.76
59802 PITT		CRAIC	-	1500	4121		4-13	111 8	1205 - 4-18 79
125 2 5:20		CRAD		15:00 19:00			4.17	PS 227	
45 K 1835		CKNO		530	-	1	4-17-14	PSSS	1500 4.07
Le 24 F5 418	PRIST-	CRND.		500			1-17-2	PS 218	18:00
1		CRNO		15.00	171.4		4-17-2	1250	3000 417-75
57.32 Piers		CAMO	-	1,500	1.12	.11	11-1	PS 213	
50 ES & 1331		CEMBO	-	1		1	1.17	PS 235	25:00-417-7
5.83 R220		CKN		15:00	4-6		4-13	PS 920	AC -11.60 -0.15.76

Incl 2

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SPRAY TIME 34				_	1 22:45 -4.7-76.	20:15 - 4-13-78	M. W. S.	-	-	86-31-7-31.81	1500-4-17-78	_	-1		# x1.45 - 1/4/4 75	1 2300 119.18	30.75	-	000		-	0080	_		-	82-61-4 0080	AF-91-1-36		\$ 24:20 - 4-16-76	\$ 22:50 - 4-18-78	5 21.35 4:16-78	r		1		•		10:00 4-21-3	-	1
VALYE		W 223	KJ. 254	PS 237	618 316	DS 236	RUNCIL	P5572	P5.239	PS 201	P5 291	(X 240	PS 24	**************************************	18.54	165 23	PS. 282	PK 292	PS 243	PS 222	PS 245	PS. 346	C\$ 247	B 248	568 SU	056 29	158 251	PS. 352	PS.253	18284	03.255	N5256	7-126-2	2-127-7	P3264	75.26.5	4226	Control	656-50	BUCK
CLENUAL BLAST TIMES DATE		1	7.2			.1	Will Kills	M-4 posts	14:00			4-14-125-411	11 11 11	18:00 - 4-17	11.00 m	4. 12 8 1.1	_	_	87.69 - 2-19	_	21.30	12 K-13	-4-18 6:50 4:1A	17.30	1300 4-18 17:30 -4-18	子が、大	17.50	17:30	27:30	3/1:30	21:30	2/:30.		00:11	12:30	15:30	17.0 0300 0.71			000
CLENNOZ	15.00 11.11	15.00 della 21.50	1500 11-0	76.00	- 13:00 d-16 21.30	1500 4-1249.20	1833 Wattersa	1500 11/1 Mich	1500 4-12	15:00 472		1500 4-12	- this to		-	The same	1300 4-8	1200 4-18	13004:4-18.	1300 H-FR	N-4-00E1	1509:111-18	1300 4-18	1	1300 4.18	1309/LAF	1		1300	1300	2	2	W/W				0900 110			
Love														Autor We					Payer			Regist				april			HENT REGITAM	Print	HEAT PESSTAN	Philip								
Meterial	640	1000	1049	2000	DIWIG.	CKMC	ET TOK	STEEL	STEEL	CRNO	STIEL	STEEL	Sheek	J'hort h	State	Steel.	CENIA	STEEL	STEEL	STEEL	STEEL	STEF	SIEEL	STEEL	STEEL	STEEL	Share	STEEL	STEEL	STEEL	STEEL	STEEL	STEEL	STEEL	or o	- SIEF	STEE!	STEEL	STEEL	CTEEL
								low	long				1	· Acres (125)	,			or ser	"	" "	",	"	1	11	7/1	11	"	"	1330	1000-p-3488			HATCH COVER	HATEL COVOR	100	- Company	2	- Some Value	Lung O glare	Jack 1 Jak
Jake ile	ECCK OCEON	X130.0 110	A CHO	Section 1	Se Se Def	c-20 (5c3c	\$ 50	BY PESSE	m 15239	C 4052-830	50435 - 18 94	Sc:19-415-39	1000 0000	Set ASSET	C642 P. J.	\$527 5528	5032-15262	SUGS PAUZ	Syer PSails	Sys Pszyl	5462 PS 245	SHLA PSAILL	SHILL PSHY	Sylvo Psave		SHSA PSASO	Sylal Psasi	Syst Passa			SUSS PS.255	अर्थ एक	7-126-9-1	2-101-2	1 5564	P3263	200	Den 1	1525G	Ascad

Miles III		Phone	ford	- Jag	-	DE-	14. 16-	Jan 7 1
366	Lune Usher	STEEL		340	4-24	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
9-16 10 15 272 DOD-P-24555	D-P-24555	c.F.E	PANINT	200	4-25 10:00	17-h	PS 272	05 DY 81-50-4
S796,14 13276	A CONTRACTOR OF THE PARTY OF TH	CFE		300	4-25 13:00	1	1	4.25-78 13:30
594 20 PSCB		CFE		900	4-15 13.00	1	PS 275_	4-25-78 NOO
196. C) 2407		CFE		900	425 13:00	10 4-25	13267	14-35-78 14:30
178.5 FR 271		CFE	-	300	4-25 /3:00	32-10	PS 271	4-25-78 W.30
5948.13 13.23		CFE		300	#2 1300	25-4-0	PS 273	05.El 84-52-h
	17-P-28E	CFE	THE PROPERTY OF	900	4-25 10:00	52-h 0	PS 249	4-55-78 10:30
	POD-9-24585	CFE	PANOT	200	4-25 10:00	25-4 00	PS 270	4-25-78 ICE 30
P.24	T. P.286	C.F.E	PART	1 800	W-25 10:00	SE-1 0	PS 246	4-25-71 10:30
		252		200	2-25 0800	25-4 X	P3249	D60 St-72-6
14.1552K		CFE		900	4-25 10:30	12.4.06	PS278	9-26-78 11:00
14.7.25		CFE		200	425. 10:30	77-1 0	PS280	0011 81-92-6
2		CFE		200	0050 52-4	32-4 00		4-24-78 Ofto
5483 Bat	St. State of St. St.	CFE		300	4.26.1300	16-4-27	psesd	4-27-78 MOO
AB. 15 231		CFF		200	42 0800	32-6 00	PS 28/	2-22-78 000
6 6 6 723		Ţ£		900	4-25 0400		P5283	1-W-78 OF
1774 K \$		CPÉ	Regard	300	4.45 0000	81.11.5	PSOT	5.130 87-51-8
M 19 5274		CFE	,	200	4-26 10:30	0 4.26	PS279	4-26-78 11:00
H2 11 15274		CFE		200	415 10:3	0 4-76		4-4-11:00
725 736		CFE		010	4.25 10:30	27-4 0	PS 287	4-16-18 11:00
		CFE		000	125.13:30	10-4-07	1	427-78 1400
M. 16 1525		CFE		oto	4.15 0800	32-4-00	PS285	4-21-78 PAC
7.13 B 27		CRMO		1000	4-26 13.35	2-1-50		12-X-14 14:45
多いろろい	Standard Comment	CRAD		10001	4-24-13:30	1]	4-26-78 14:20
938.29.5293		CRMD		1000	4-24/3:30	0 4.36		4-2-7 14:35
18 3 75296		ay y		1000	4-24-0930	16.4	1	4.37.7 PO:50
18.28 15.25		CRAD	-	1000	426 13.30	0 4-26	-	4.2.7 W.30
98.H 75.291		CRMC	The Party of the P	2001	1-14 13:30	12.40]	4-26-78 14:35
6297	T-P-286	CRMD	10 x	1000	124 1300	1		4-27-78 1400
		CKAO		1000	4-26 13:30	0 4.20		4-26-78 14:30
98 - 82:0		CKMB		1000	4243:30	02-4-60	1	4-26-78 14:30
43694.17 Det		CKND		1000	(K:E/7-h		-	4-25-74 14.3
1% 2 N 389		CLAID		10:00	426/330			4-26-78:1935
0x 2/2 3/0		C Tho		/3:30	4-26 09:30	1 22	PS 305	4-27-74 11:00
17614 15 263		CKAD		(3:30	4-20015	5 4.27		V-30-35-08-30
916 23 PX		CKMD			4-20 0715	5 4-27		4.37 X CS15
ALCO BY		C mp			4-26 0115	. 1	RS 3/4	
136.31 15.30		CKMO		13:30	4-4-07.15		-:	427 Y CSF5
4%.12 13 34	Trp-2915	CLMD	"松松"	13:30	4-24 1300	C2-4-0	-	2-2778/400

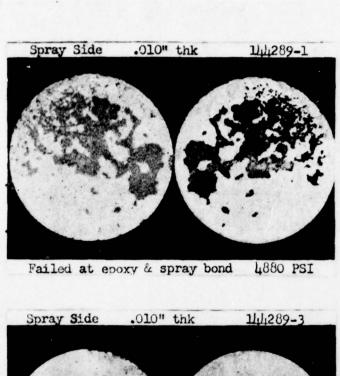
		ļ	Clean	Cleaning Time	Blasti.	Blesting Time		Spray Time
Value Ne.	Material	Level	Pate		nite	1	Make No.	1.7. t
54 F 4 F 5c2	CKAID		13:30	4-26	09:30	4.27	P5302	4-27-78 10:30
4x.27.530	CRAID		17:30	1-4-11	4-16 09:30	4-27	PS 310	4-37-18 10:55
5976. B 13.12	CKMB		13:30	4-24 0930	0530	4-32	PS 3/2	4-37-7 10:30
5438.18 13 315	CRMO		13:36	4-36	4-36 0715	4.37	PSSIS	4.27-19 C'15
49%. ICF 309	CKKO		13:30	11-36	11-36 0715	9-27	PS3C9_	4-27-18 G:15
5 9 58 7 15 3 07	C.C.MO.		13:30	704	436 0715	4.27	PS307	14-27-781815
59% 5 K 37	ckmo		1380	1.2	4.2 0930	427	PS3/7	4-27-78 11:0c
5976 6 8 316	CKND		13.30	1.2	4-2094S	497	P\$3/6_	JE:0 31-16-4
54% 26 1540	CENO		13:36	43	42 09:30	4-27	P5 308	4.07 FT 10:31
59% 1513 X5	CRAD		13:30	4.34	42/3:30	4.27	PS305	E. 11 81-16-1
59% % 576	CEMO		13:30	43	436 13.30	4-27	N. 235	4-27-781430
5 98.55 N 13 TT-P-29E	CENTO	HENT RESET	1330	434	434/300	4-27	P\$3/3	4-27-78 1400
	CRAID		13.80	436	436 275	1.27	PS.311	4.22-NEK
19% 18 P3 de	CRNO		10:00	4-27	4-27 08:30	4-18.	P\$320	126087-85-4
815.218.318	CKMO		10:00	4-27	4-27 13:30	- 42-h	PS 3/8	4-28-78 MOD
4 M2. %. 15 324	CRAO		10:00	4-21	4-21 08:30	1-28	PS 324	4.28.7 10.3
5 942 H. KTB.	CENO		10:00	4-27	4-27 4-28	0:730	PS 326	4-28-TY 0930
5942 # 15327	CRMB		10:00	4-2)	87-7 (2-1	0:830	PS 397	4-28-TY 10:00
5942.45 DS22	CEMO	•	1000	4.0	4-114-28	080	PS 322	4-28-78 09-55
59 %. 4 CS 36	CRMO		1000	4.17	4-27 0:730	82-4	PS 3/9	4-28-78 0.550
649: 13 17 ES	CKMO		1000	4-17	4-27 07:30	85.4	PS 335	V-36 08:30
99 F. W. B. 321	CRMO		1000	4-27	08:30	4-28	PS 32/	3160 82-1
992.59 PS 323	CKM		100	4.27	4-27 0:830	4-28	PS 393	458 0900
5942-39 PS 536	CRMO		13:00	4-37	13:30	82-4	P5335	4-36-14 MOO
S942-28PS 347	CRMG		1300	4.27	05:20	30-6	PS 347	1.35 06:30
\$942-30PS \$33	CRMO		13:00	4.27	A.57 6:8:30	87-6	PS 333	4-28 O97.
5942.74 (5 337	CRMG		/300	4-22	0730	86-1	PS337	V-38-78 050
Squ2 35 PS337	PRMC		1300	4-27	4-27 08:30	.82-6	PS 339	4-28-78-09:30
Squ2 -21 PS 334	CRMO		1300	4-17	0730	4-28	PS 334	4-36-78 2500
5942 53 85332	CRMO		·4/	4.57	13:30	3206	PS332	4-25-78 MOO
S142 11 PS348	Cemo		1300	4-27	4-27 07:30	4.28	. PS345	4-28-TP @35
Squz.73PS 334	CRMO		(30	4.27	05:20	4-28	PS334	4X-1 09:30
721 SQ 51. CMP 9	CAME		1300	127	08:30	182-1	PS 33 6	4-28-78 09/3
947 . 19 DK 243	CRMG		1300	4-27	0:4:30	4-28	P3343	65:01 8-82-4
Sq42: 3005341	CRIMG		1300	+27	0:730	81-4	PS341	4-28-78 05.55
594217 PS 342	CRMS		8	4-17		182.6	PS 342	W-28-78113
S942.33PS 33I	CRMG		1300	+27	10:30	12-4	PS 331	4-38-11 NES
594275P534B	CRMO		(300	4-37	10:30	4.28	PS 308	428-78 11:30
5942 29 65340	C RM6	-	(1300	4-27	10:30	4-28	PS 340	428-79 11:30
S942-42P5338	CRNO		1300	14-37	13:30	82-6	PS 338	4.28-16 1100
The state of the s	0000		1200	433		2-26	Do sad	190 90 301

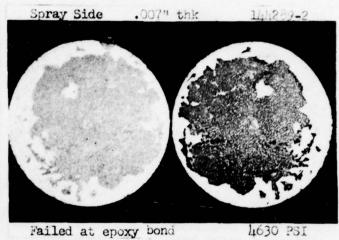
WALVE.		MATERAL LEVEL	CLERNING.	BAASTING TIME ! DATE	VALUE NO.	SPRAY TIME	Fime
S442 1.4 15 341		CRMO	PC-34	27. OF CL.78	P.S 200	100.00	5.1.30
542.251335C		CRMO	1000 4-28	13.30	15350		1-88-1
59R. 26 15359		C C Mo		1300	P5354	1	5-1-75
592. 52 7357		CRMB	1	07.30	PSASS	1	5-1-78
594.8 PSSS		CEMO	1		PSSSS	1	5-1-78
5942 F5316		CFMo		97:30	PS 346	1	5-1-78
542.25 Kine		CEMO		07:30	PS 25.2		5.1.78
Car 9 1833		CRMO	1	02.20	PS31.3	1	5-1-78
5002 LA 15357		CRMO	1	20.21	05357		4.36.70
ANZ. 41 15356		CEMO	1	02:20	PSACE	1	5-1.70
1942 Te 15 75		CHANO		0750	PSSCI	1	5.1.38
442.10 1338		CKNO		02.20	PSACE		6.1.78
SOUT 1524		Cemo		1	827.0		00.1.2
5947.71PX		Cemo		11:50	Prace	1	5.5.78
C. 27/23. C. C. C.		0400			De 27.7	1	2
WY 11 CVP2		owa,	-	15.00	Race	1.	11.70
1917.7 KEL		0000	1	200	052411	1	200
5947 31684		Owo U	1	13.80	PS 361	1	21-1-3
AV2.275348		CRMO		00.80	PS 34.8		4-1-7
35 X 12 109		Cigmo		02:11	8 366	1.	5-3-78
442.511.343		Chimo		00.61	PS 24.2	1.	5-1-79
5947-4755362	1	CRMP		02:20	PS 34.2	1.	5.2.7
12,0 137		CRAC		1300	PS374		5-5-7
142.675376		CRATO		1300	PS 376		5.3-78
A2 7 1373		CRAO	1-3 X 30		PS 373		5-3-78
442.6 B312		CRANO	1-5 25:80	_	PS 378		5.2.78
HP. IL BYN		CEMO	08:30 54	_	P5369		5-3-79
14.50 P. ST		CKNO	1 08:30	1300 5.2	PS 370		5-2-78
142.57 [371		CRMO	18:30 54	13:00 5-4	PS371	1	84-4-5
THE OF PIR		CRMO	15 08:30 54	87.30 5.2.78	PS 375		5.2-78
57E B 5F	Low Valer	CFE	11:00 5-1	27-478	PS378		5-8-76
Sree B3X	たって	CFE	1:00 1:01	81. 8. S COSO	P5330		5-4-75
mig PSZY	the of the	CFE		12:30 5-11-18	PS 329		5-11-7
S	ところ	CFE	1-9 00.11		PS328		86-11-5
	2	CFE			PS 385		82-45
П	me coler	CFE		81.8.5.00.7/	PS 384		5.8.76
1	July Ophic	CFE	1	SC-100 0080	68889		27-1-0
. 1	Love John	CFE	1-3 20:11		P338X	14.30	5-11-2
5595 P) Ec	37	CFE	1.50 5-1		13380	.,	5-4-78
	3	CFE	1-5 act	82-4-5 0080	065 Sti	800	82-ha
					-		-

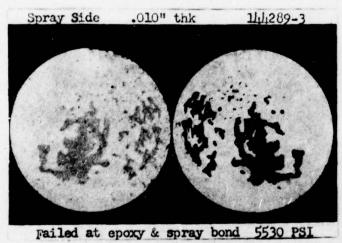
				_	Builande .	
Valve No	Material	Level	times ate Time + Date		Time & Date	i
5.72.5815 EJ	CKMD		13m 54 11:30 5-3-78		12:30 5-3-78	0
5972. AO 13 SEI	CRMO.		13:0 51 11:00 5.2.78	_!	11:35-5-278	78
X42.5. 15.30	CPM	Payent	R. 4-7 080 5-4-18	.!	84-4-18	80
SA2.72 D.36	CKNO		12-5 W:11 7-5 WES	PS 386	1:8 5-2-78	28
FR. 4 13 373	CRNO		13.00 5-1 13:30 5:3-78	15393	14.45. 5-3-78	8
M42. P. B 377	CRAO		13CD 54 1300 53-78	PS377	1400 5-3.78	2
SA2. 5 18391	CKNO		B.W. 5-107:30 5.3.77	ps 391	8400 5.3.78	20
5972,2 15 355	CRADO		5.1	PS 396	1	*
R. SU B. B.	CRMO		5-1	155389	1	
912. 21 3 42	CRAO		5-1	Ps 392	11:30 6-3-79	2
SHE'N B371	CKNO		5-1	PS 379	"	2
SAR 77 183%	CEMO		5.4	1		20
MR.3 B34	CRMD		54			
942.32.PS 410	CRESO		5.7			0
5942 92PS 949	Care		5.5			00
5992.38.05 408	CRAG		5.5		86-8-3	
5942-22 /5 403	CRMG		52			38
5942-1 15398	CRMO					28
2042.6873.402	CRMO			_		.78
SPYZ. SDPSHOV	CRMG		5-5			84-
ton SAKS thes	CRMO			Ps veg		-78
5942 65 15397	CRMG		190 5-2 3:30 5:3.78	FS 397	14:45 5.3-78	-78
5942-71 PS406	CRMC		1946 52 1000 5:3:78			3-3-78
104541-1069	CRMO	4.	8-4-5 05:01-5 mg	10450	1100 5-5	5-9.78
5942.34.8399	CRMG	,	CARD 5-2 1000 53.78	PS 399	10:30 5.3.78	2
5945-78 PS465	CRMG		1900 5-2 com 5-3-78	1	09:50 5-3-78	34
5997 49 1590	CRMO		gard 5-2 0500 5-3-79		Od:45 5-3-78	-28
CINSALS BALS	GRMO		13:00 6-2 prod 5-4-76	Ps 417	0-5 34.60	86-5-5
S 948 SUPSULD	QRMO		1300 5-2 79:30 5-9.78	PS 420	1000 5-9	2-8-78
S448-42FS 4W	CRMO		1000 5-2 1000 5.398	PSAIN	1100 5.3-78	34
Squ8.38 PS415	CRMO		1300 5-2 1000 5-3:75	PS 415	N:30 5.3.78	20
5948-56-PS4IP	CRMO		1300 5.2 0800 5-11-13	1	100 5-11-2	80-
5948.37 B43	CRMO	-	1300 5-2 0500 5 4-76	PS 413	Sr. 9-9-78	٠.
5948-12 PS411	CRMD		5-2 0800		81-01-5 0180	30-
5948-23 FS 416	CRMO	1	-		(6:30 5-1-7)	2
5448 - 40 PS 418	CRMO		1300 52 0000 54-78	81h Sd 1	1-11-5 004	11
5948-52 PS#12	. camo		0050	PS 412	8 C-5-5 0180	
14.33.01%	CRMS		1300	1	1400 5-10-7	28
246.8 P.O.	CRMO		25	_		8
48. C. D. H.	'I CAMO	-	St. 101.30	PS 443	10:30 5-4-78	
			1000			

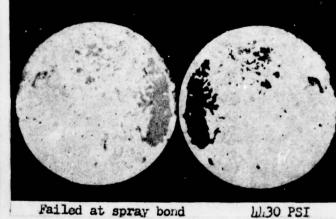
一 一 一 一 一 一 一 一 一 一 一 一 一 一 一 一 一 一 一		35 -	Cleaning	Blesting	*		String
Valve No.	Material	Level Time + Date	+ Jate	Time	-Time 9 Date	Valve Ab.	Tine + Pate
5448.37 15425	CRMO	0000	5.4	0800	87-6-5	75.425	8.4.5 SE:30
5448. 35 1547	. CAMO .	080	2.4	08:30	5-9-18	PS447	10:30 S-9-7
5418. 27 15 421	CRMO	0000	2.4	0000	5-111-78	12451	700 5-11-X
549.25 1541	OMAC	0000	2.5	ocas	8-11-8	141	X-11-5008
948 - 28 FS 4651	CRMO		2.4	paso	84-11-5	15451	900 511X
5418.57 175 444	CRMO	040	1-5	800	5-10-78	PSWU	1400 S-10-7
F#8.43 B 129	CRMG	0000	15	080	5-10-78	15429	8-01-5 OSBO
510. % P 938	CRMG	Can	25	1300	5-10-79	PS 134	1.00 5.10-1
548.50 15427	CRMS	0000	2.5	000	2.9-78	1000	87.50 59.70
5148.32 15437	CRMS	0000	5.4	0030	5-10-78	25439	06355.407
5 948-63 PS428	Cremo	000	6-0	0000	8.6-5	PS 42.8	AP-30 CB-X
5948-81 PS456	CAMO	000	5.4	0000	5-11-18	05450	211-5 2-11-5
5948.45 PS423	CKNO	0000	7-5	02.00	5.9-78	200	NO. 20 C.9.71
5948.31 PS435	Ceme	oaxo	1.5	0000	\$1-01-5	PSUBS	0845 5-10-1
5948 61 PS 440	CRMO	000	5.4	1400	5.9.78	15440	X-5-5 068
SAYE . 24 PSAyz	CKMO	0360	54	1300	5-10-78	PSHUZ	1400 5-10-78
5948-18 PS 437	CRMO	0000	15	1400	5-9-18	PS 437	150051
348.62.73.845	CRMO	080	1.5	1300	5-10-78	PS MYS	14005-10-2
5948-34 PS 433	CRMO	0000	6.4	0880	84-11-5	PS433	84-14-16
5948-34 PS 444	CRMO	asso	6.4	0080	5-9-78	PS 446	25.5.0
5948-49 Psuze	Cema	080	1.5	0000	32-01-5	PS 432	D8:30 510-7
5948-47 PS452	CKMO	ano	2.4	1400	5-7.75	psysa	1500 5-9-73
5948 -55 PSWg	CRMO	000	5-4	0800	\$7-01-3	PSWVE	21.01-5 2180
5748-36 15430	C CRNO	88	5.4	coso	82-11-5	PE 430	8-11-5 00PO
SAMB-38 PS 426	Ceno	3	1.4	osso	5-10-78	P5 406	10 900 5-10-7
6949.60 B424	CRMO	0000	5-1	0011	5.9.78	15424	15.00 5.97
21/8/5/12	CRMO	0000	5-4	0800	81-01-5	Ryzz	C-01-20 5-10-7
5948-4475434	CRMO	aus	*	1300	82-01-5	P3 436	1400 5-10-18
The same	STEEL	11.00	5-11-76	000	81.11.3	PSHSY	10:00 5-12-7
2954 PS 453 Juny Dulle	STERC	11:00	V-11-5	000	5-12-78	P5453	F-51-5 6001
					T		-

12





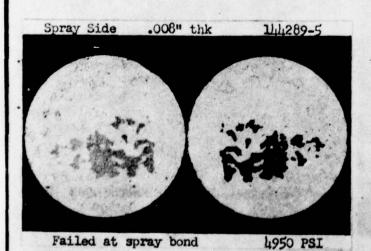




.009" thk

Spray Side

114289-4



Pulled Tensile Specimen Photographs

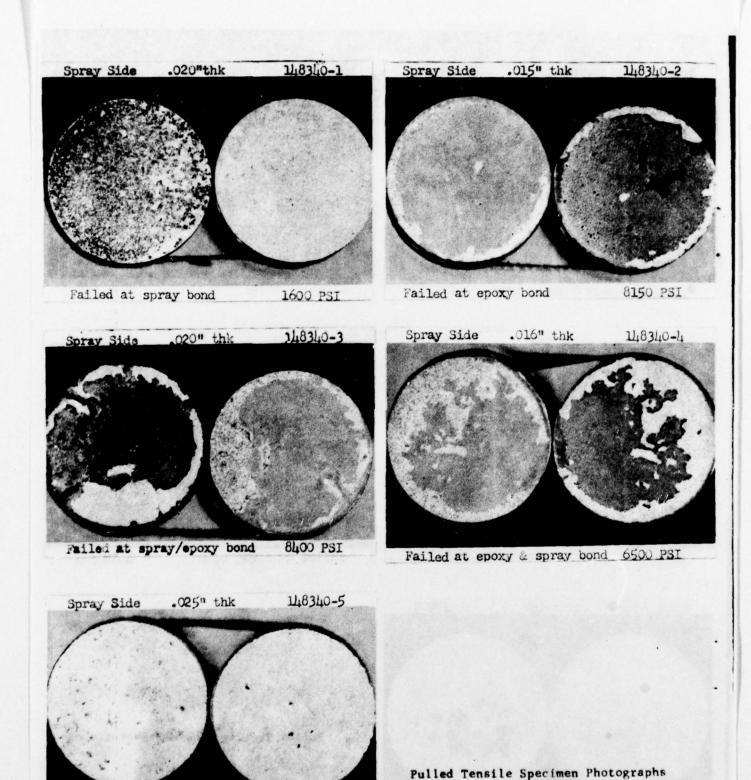
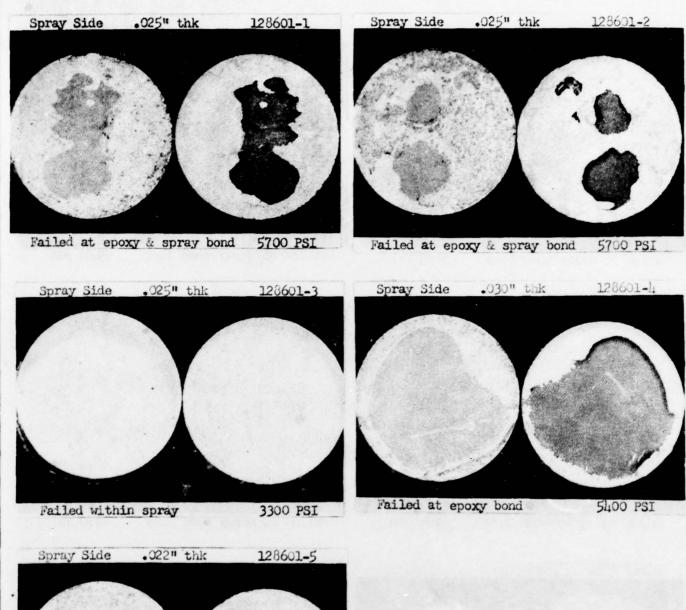


Figure 2

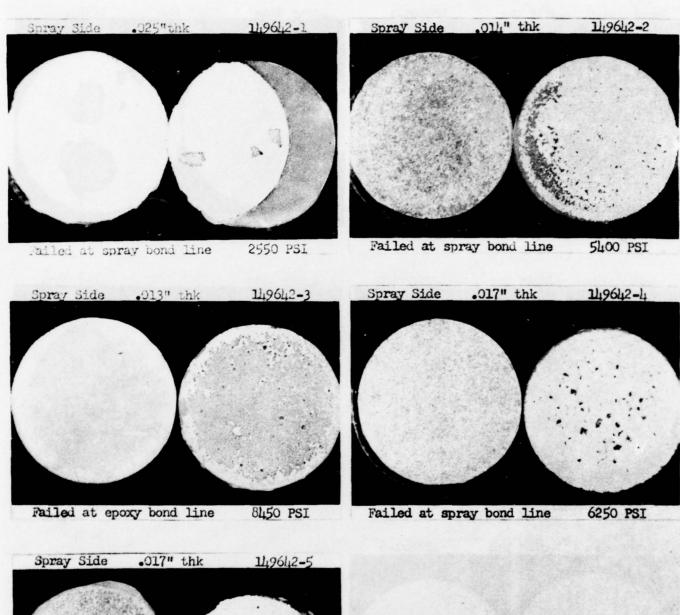
6200 PSI

Failed within spray



Failed at spray bond line 7600 PSI

Pulled Tensile Specimen Photographs



Failed at spray bond line

Pulled Tensile Specimen Photographs

5900 PSI

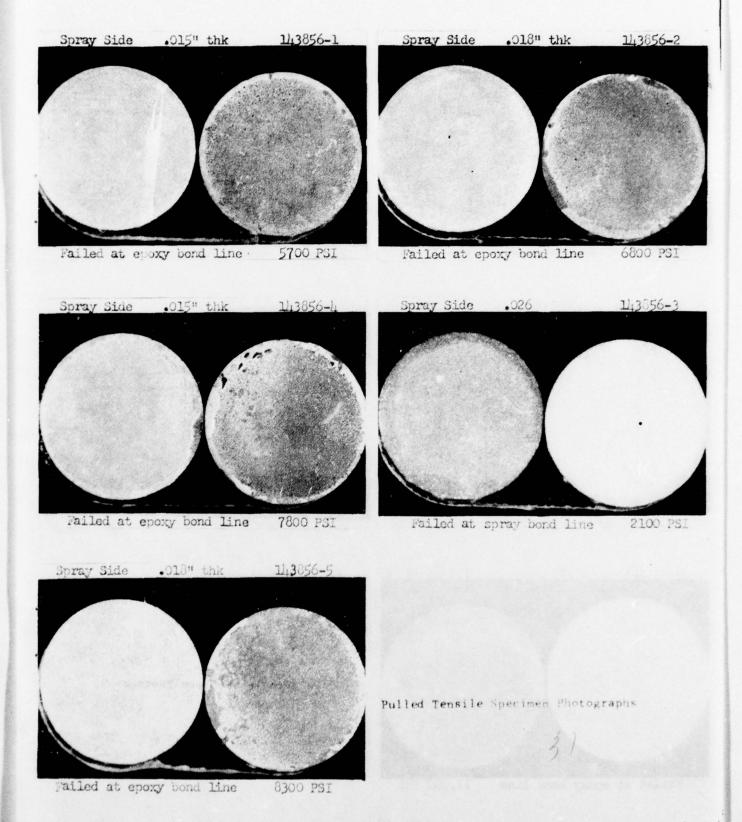


Figure 5

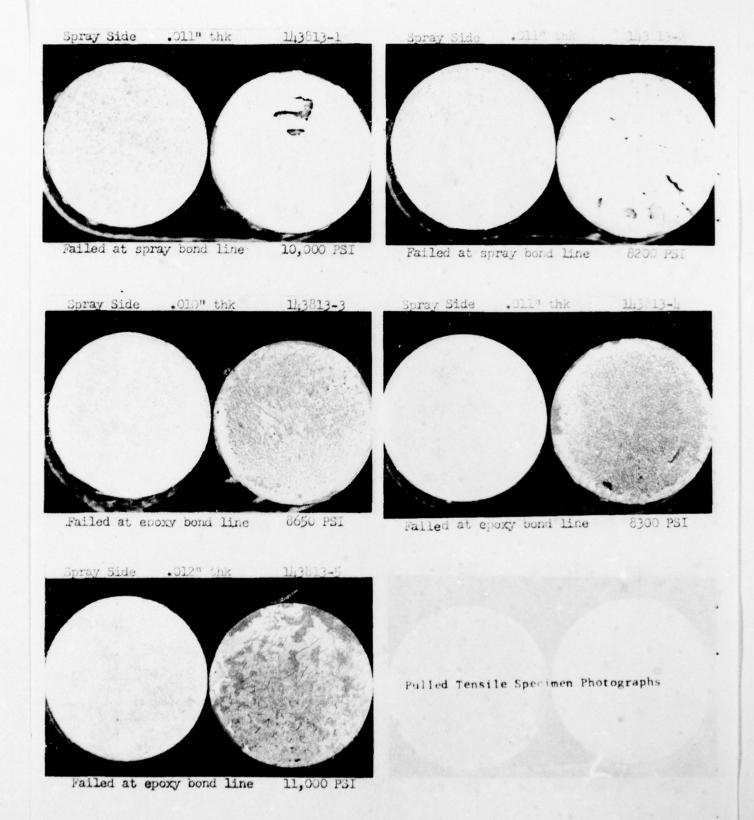
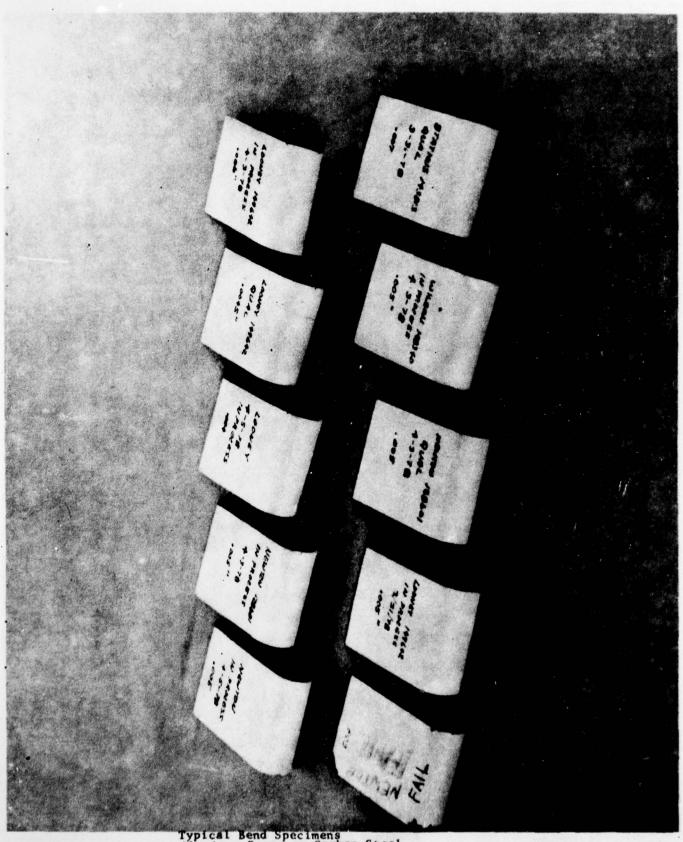
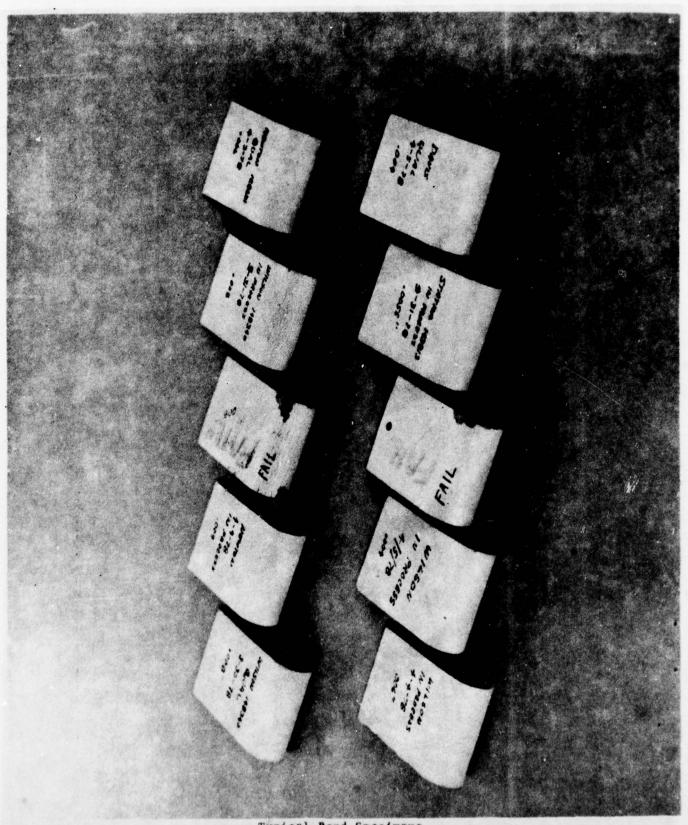


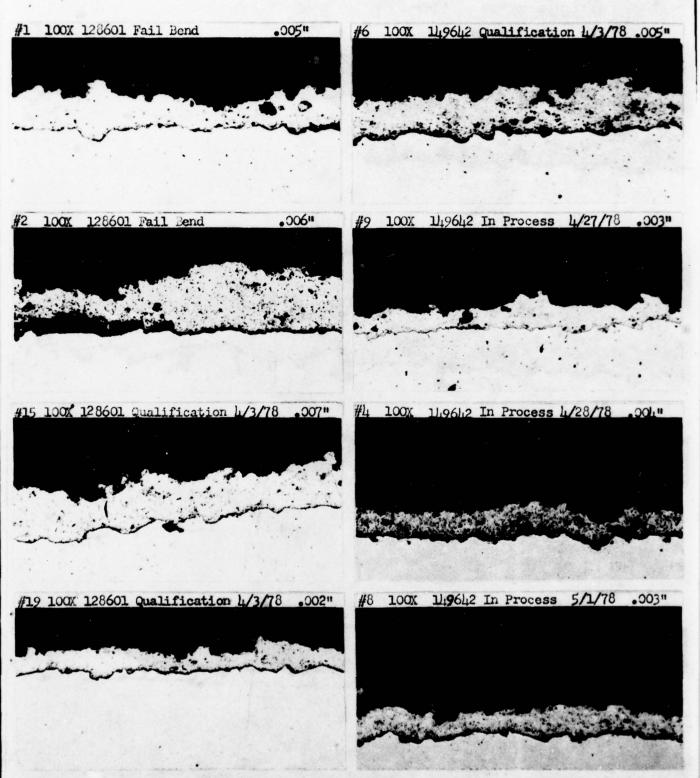
Figure 6



Typical Bend Specimens
Aluminum Spray on Carbon Steel
Figure 7



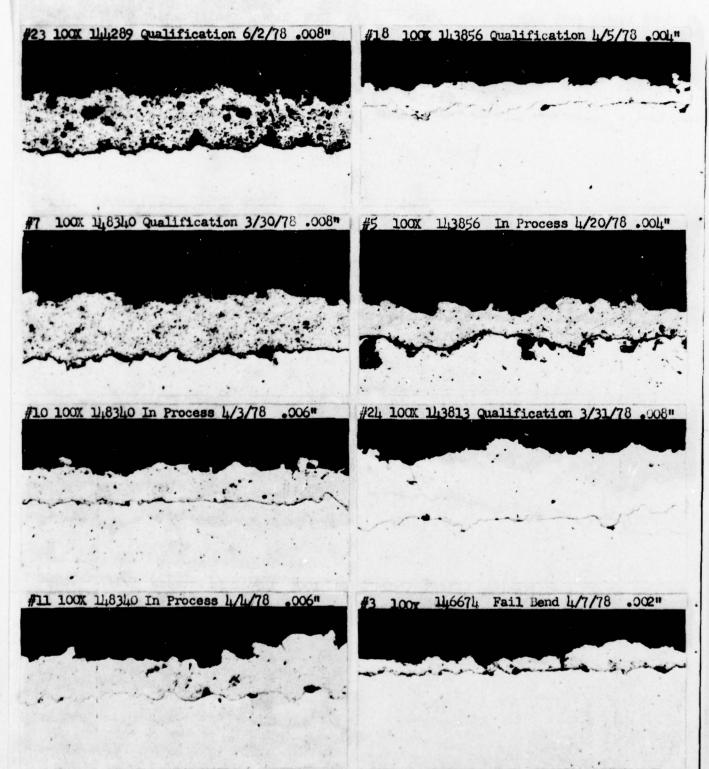
Typical Bend Specimens Aluminum Spray on Carbon Steel Figure 8



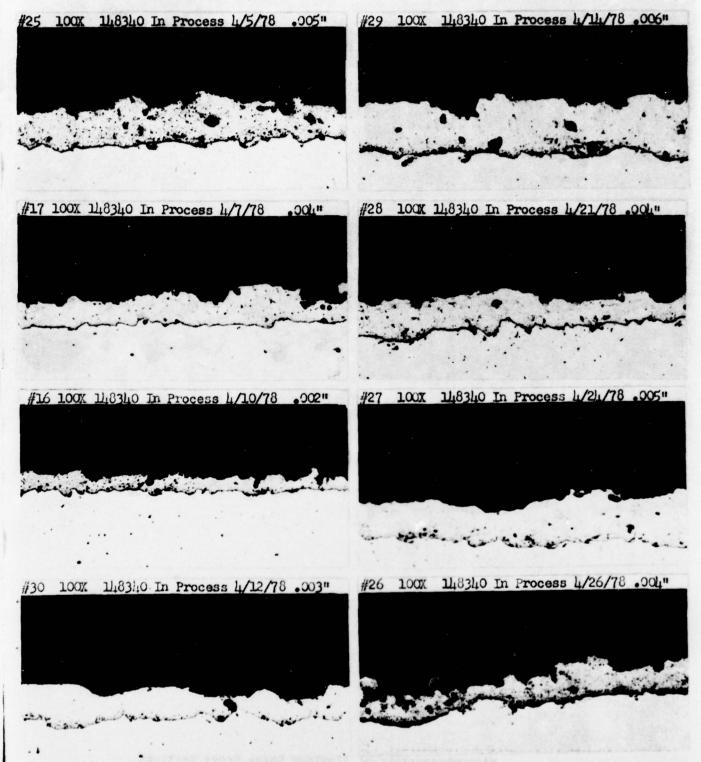
Carbon steel substrate is the light colored lower portion of each photograph

Microphotographs of Aluminum Spray Cross Sections

Figure 9



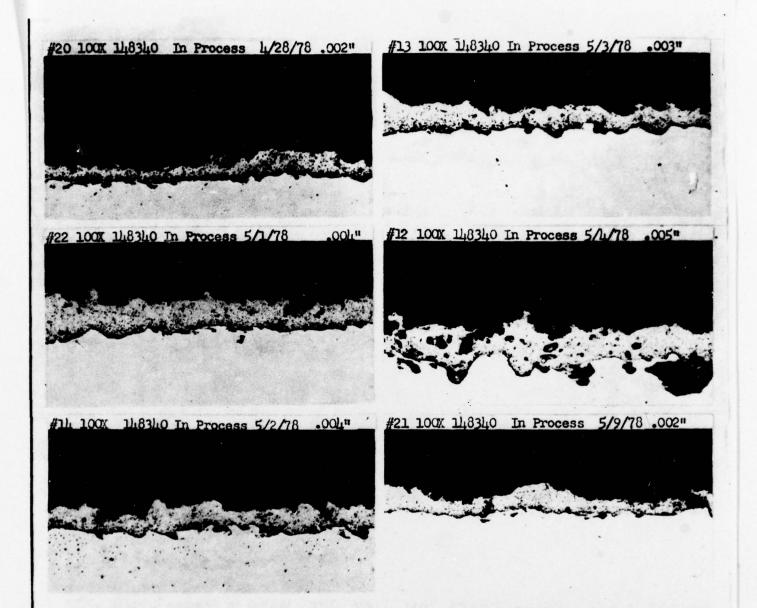
Carbon steel substrate is the light colored lower portion of each photograph
Microphotographs of Aluminum Spray Cross Sections



Carbon steel substrate is the light colored lower portion of each photograph

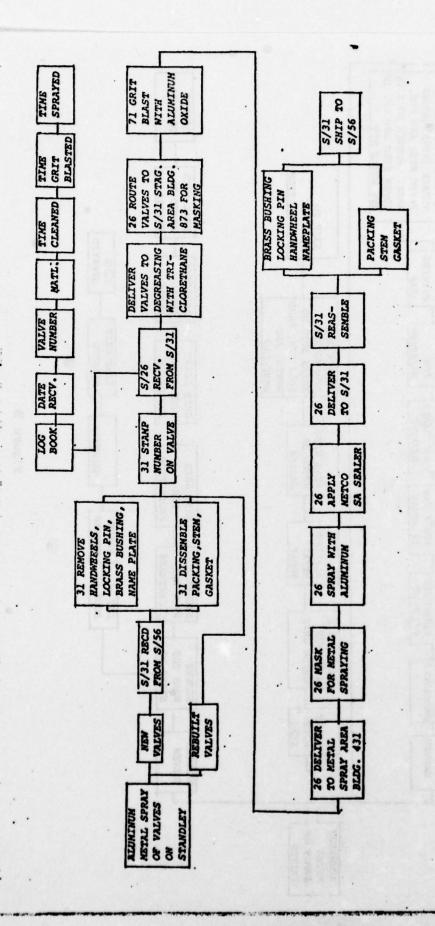
Microphotographs of Aluminum Spray Cross Sections

Figure 11

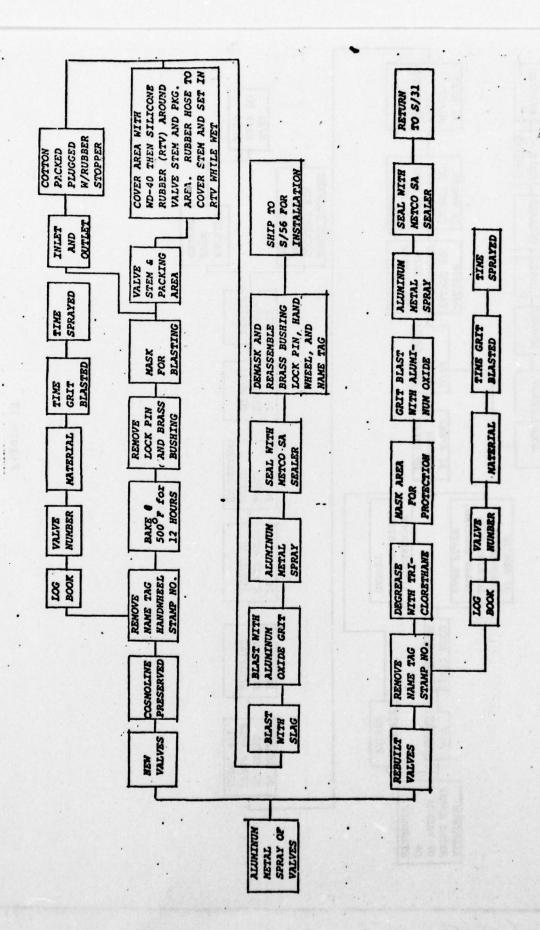


Carbon steel substrate is the light colored lower portion of each photograph.

Microphotographs of Aluminum Spray Cross Sections
Figure 12



Pigure 13



Pigure 14

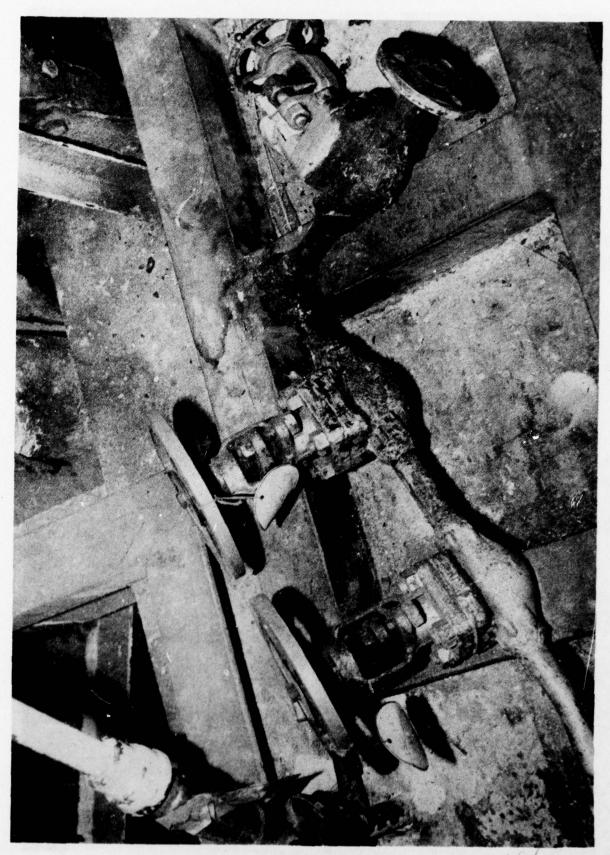


FIG 15

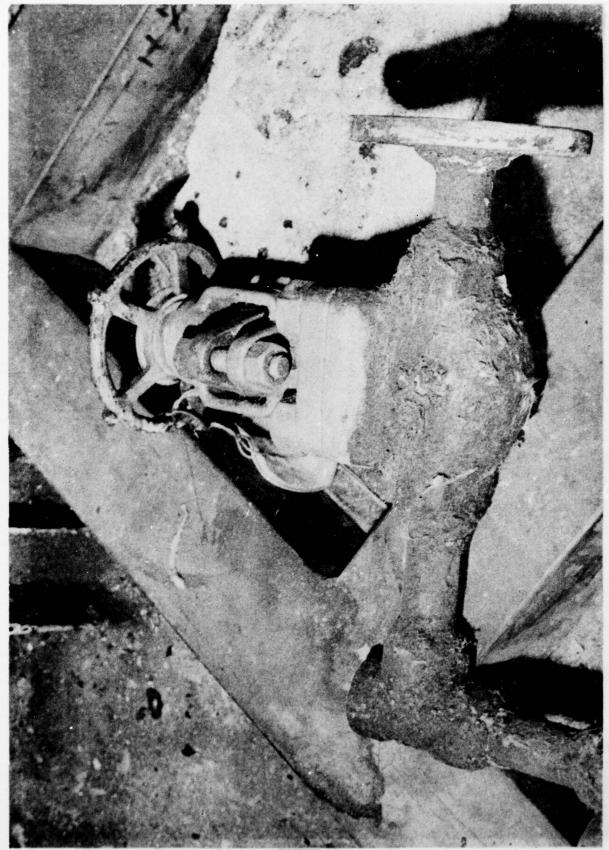


FIG 16

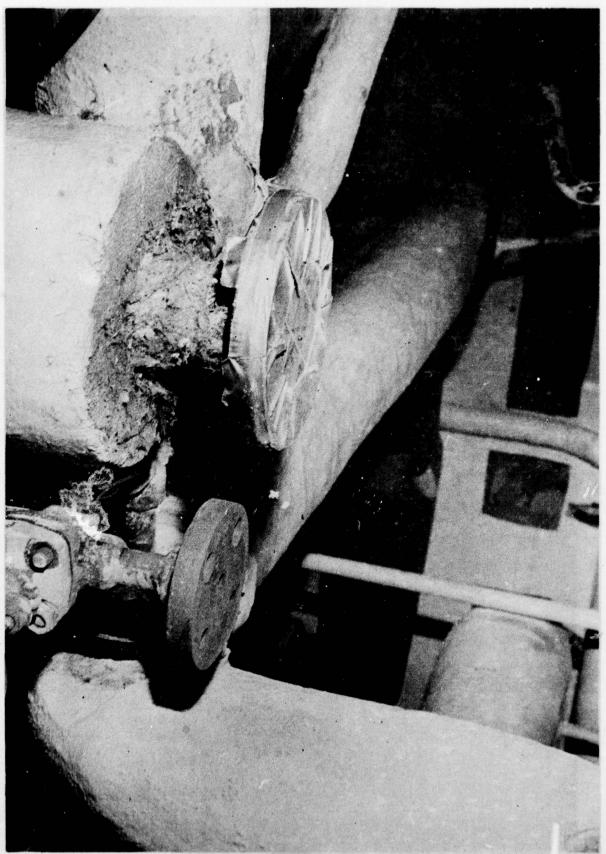


FIG 17

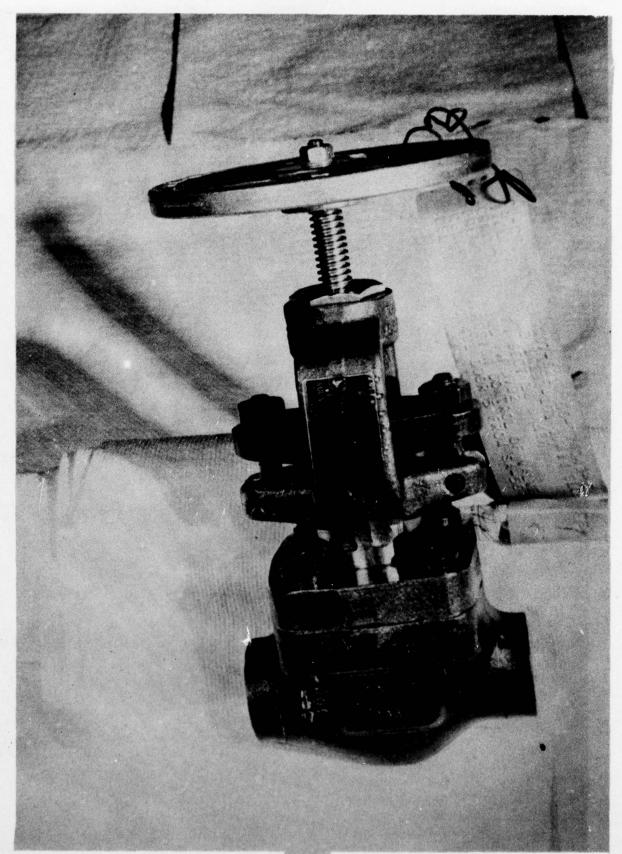
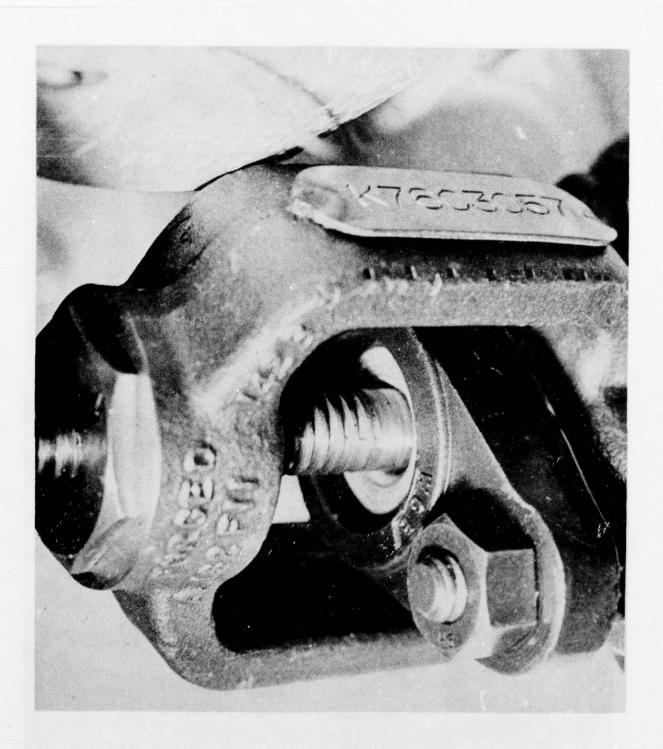


FIG 18



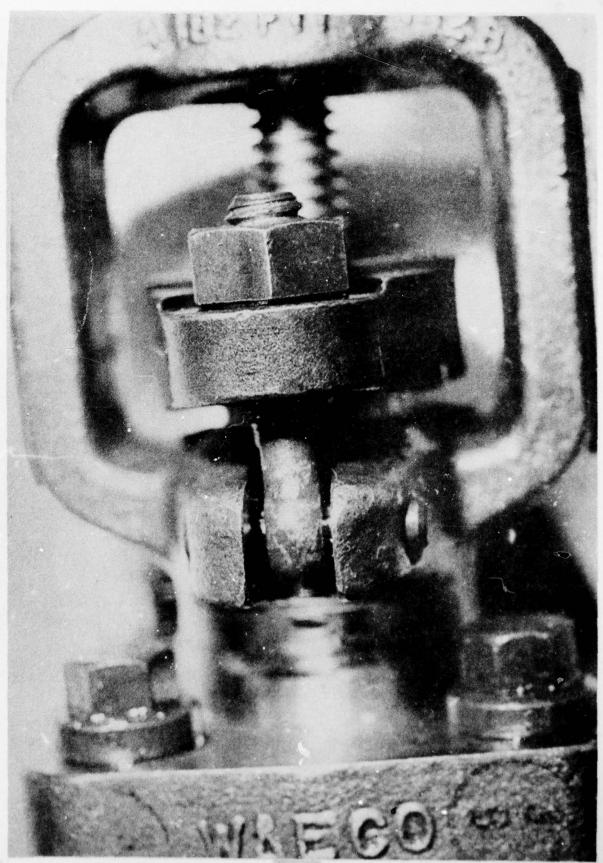


FIG 20

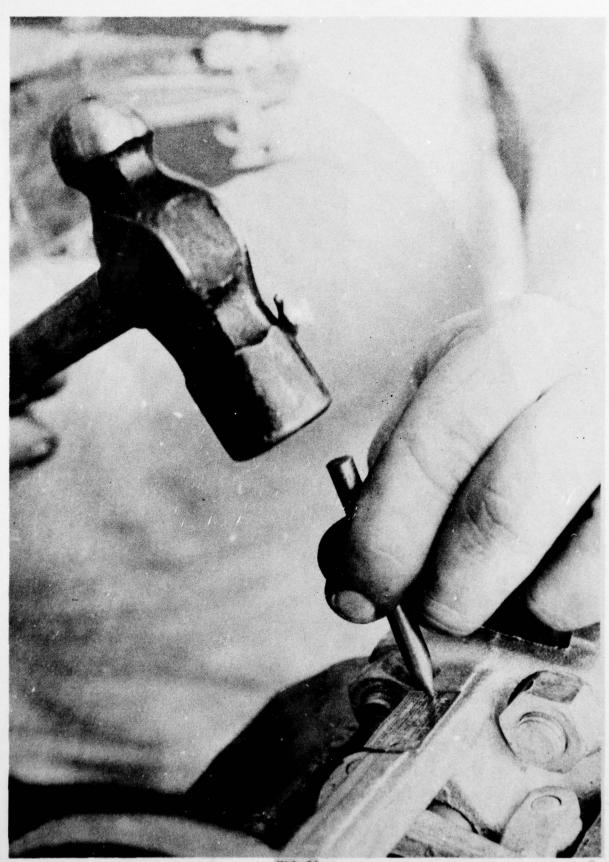
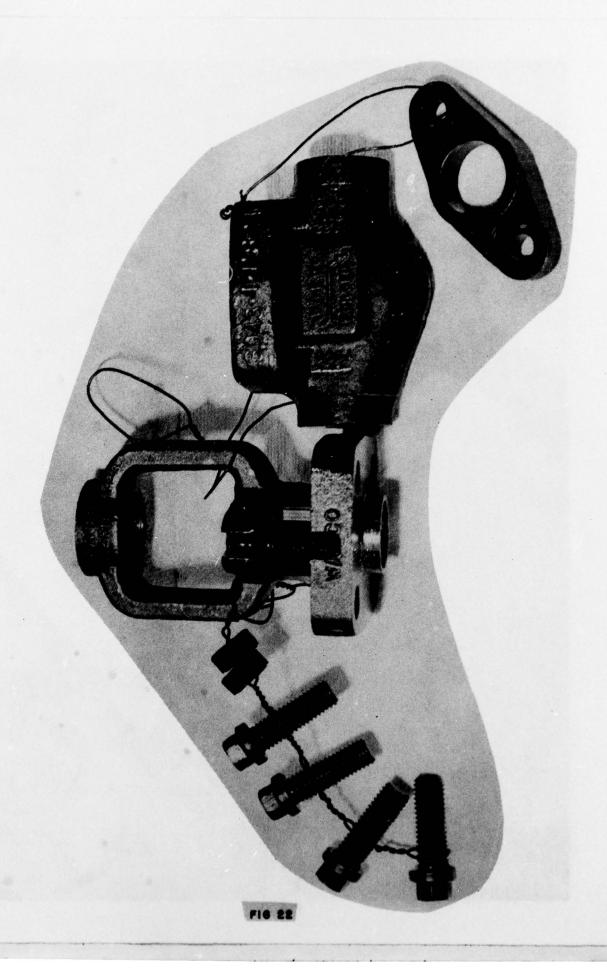


FIG 21



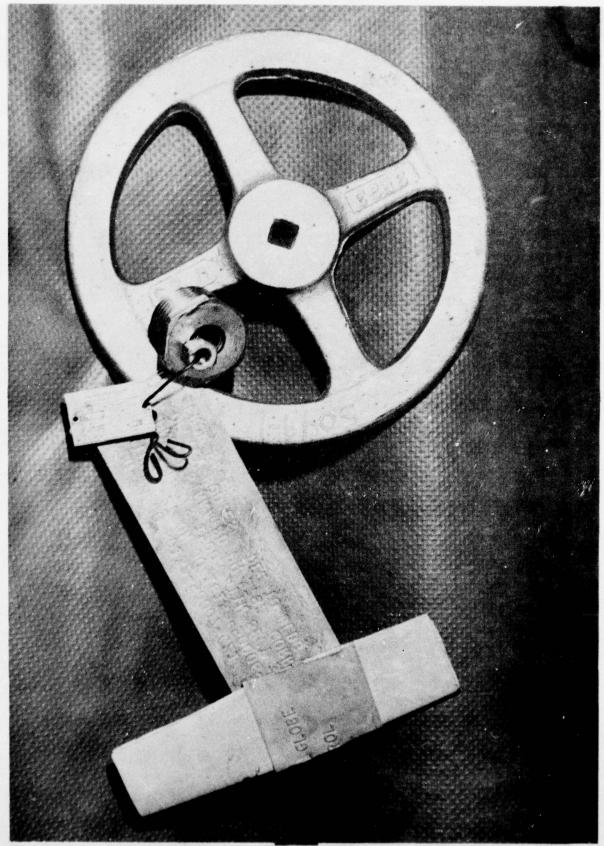


FIG 23



FIG 24

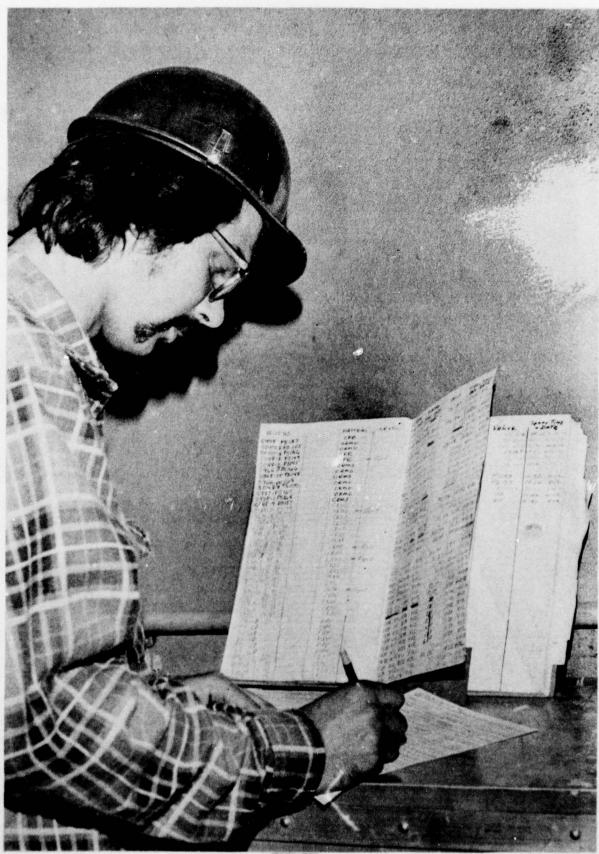


FIG 25

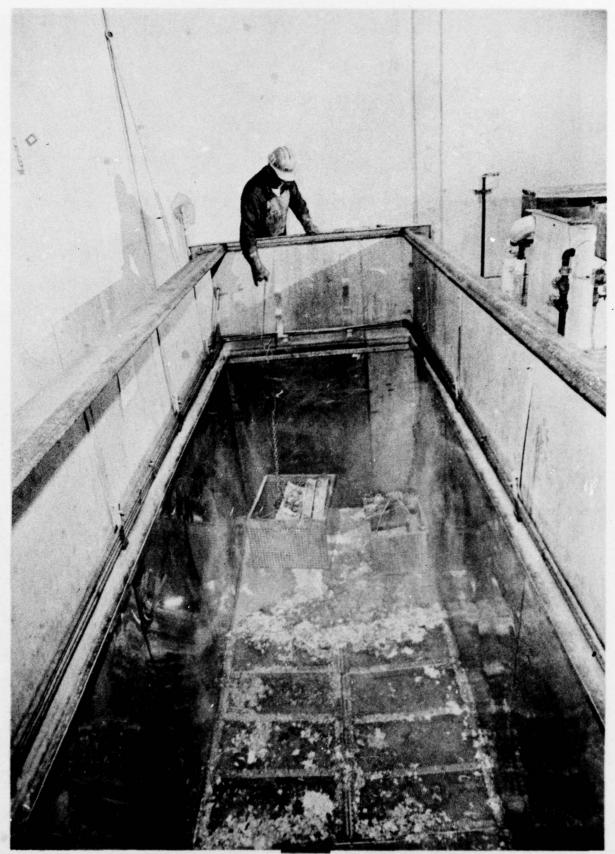


FIG 26

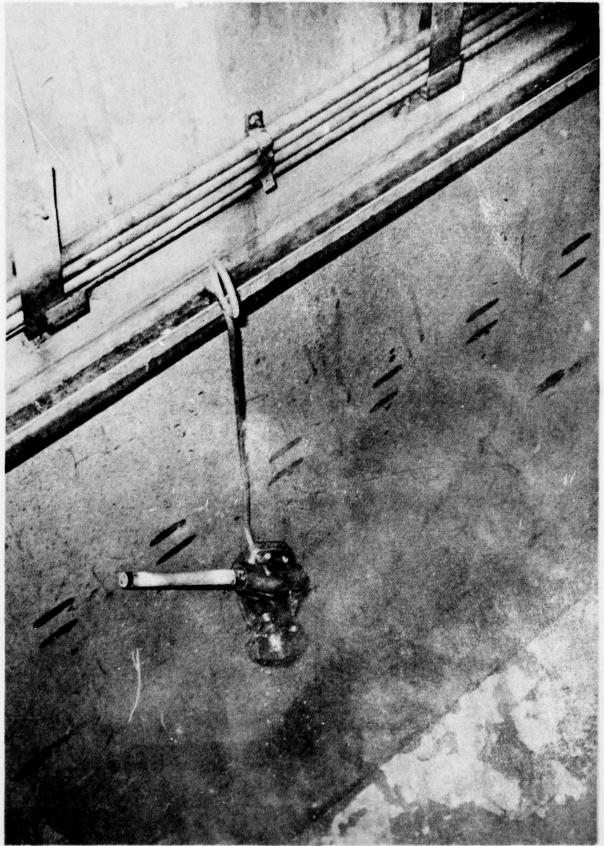


FIG 27

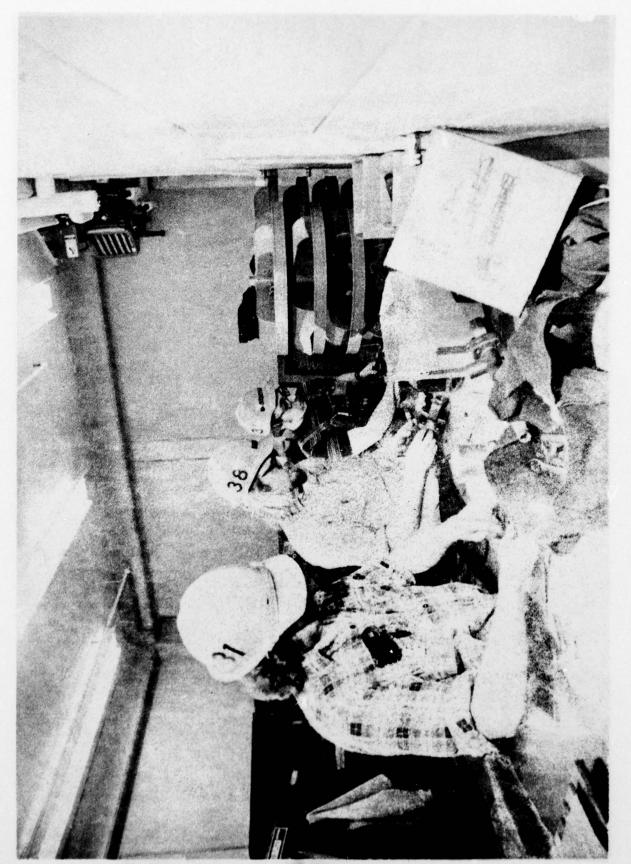


FIG 28

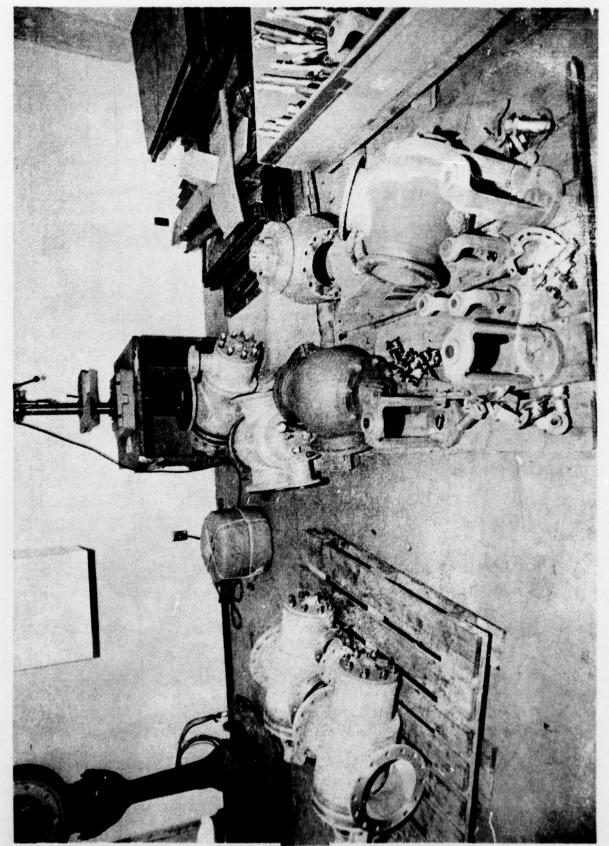


FIG 29



FIG 30

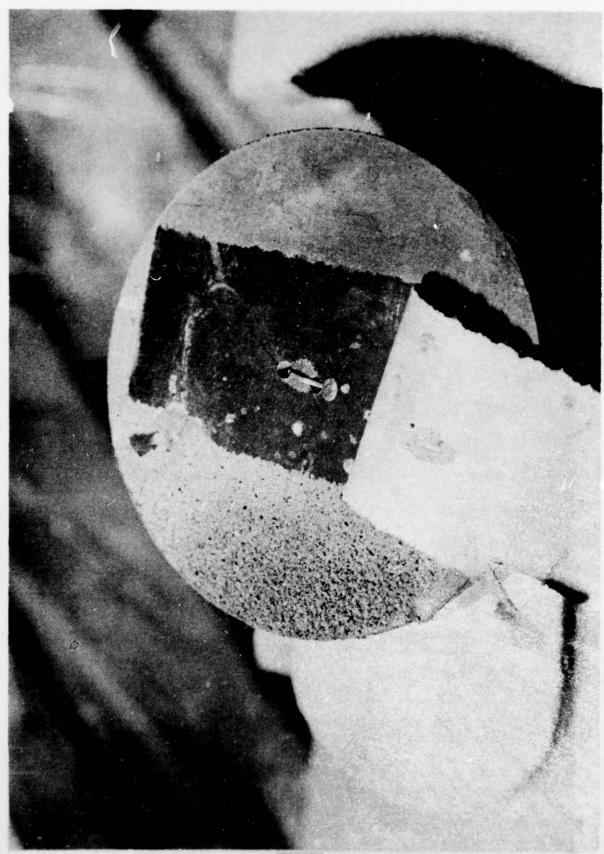


FIG 31

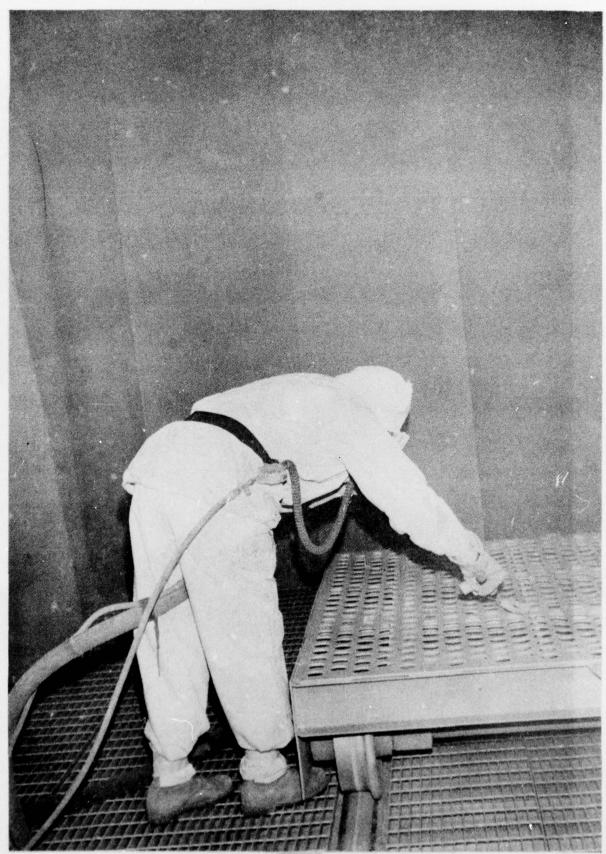


FIG 32

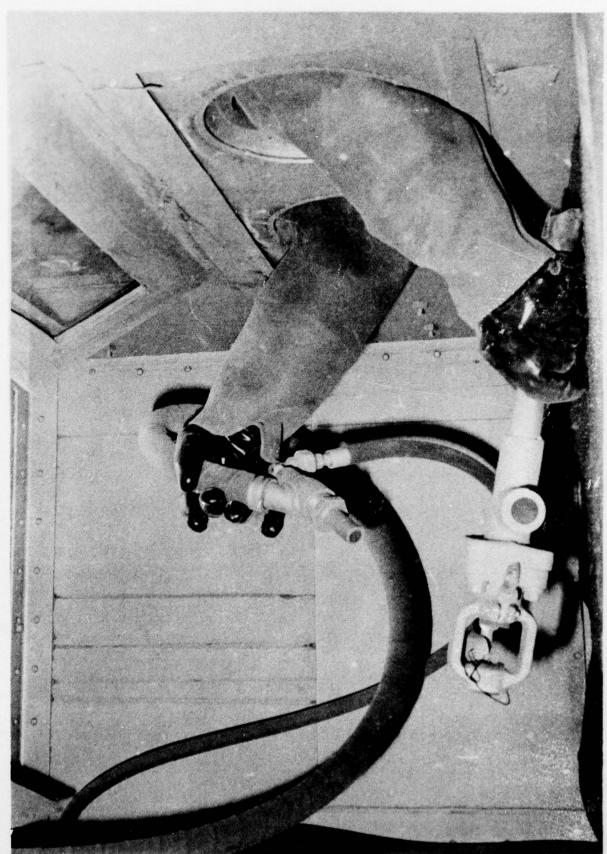


FIG 53

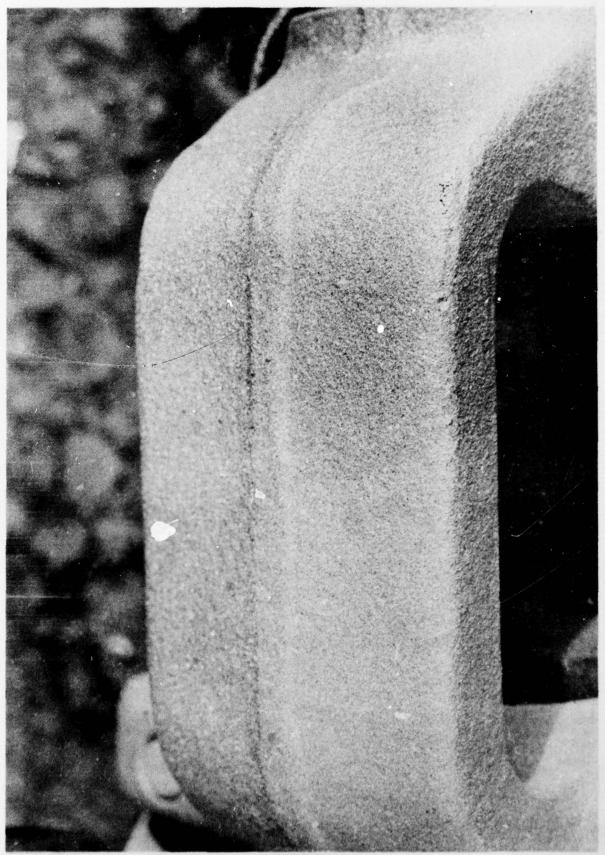


FIG 34

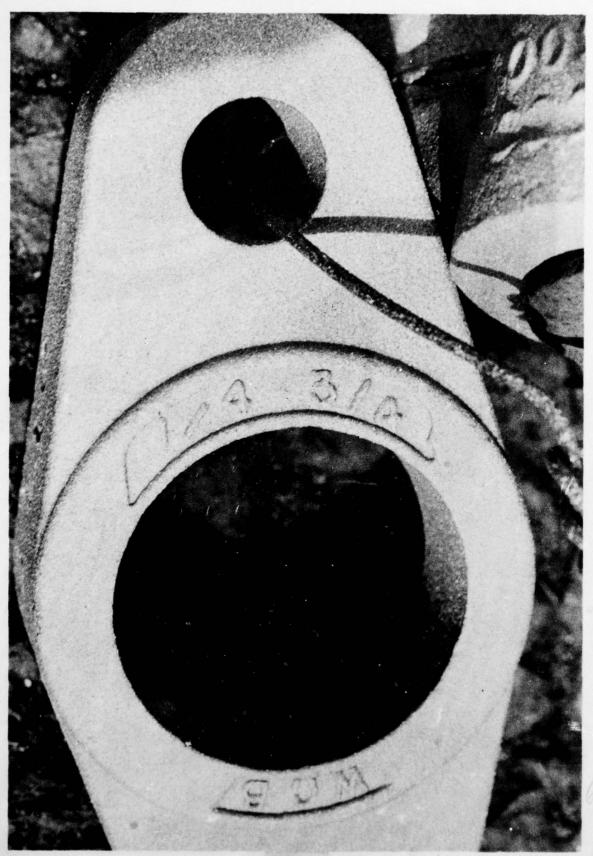


FIG 35

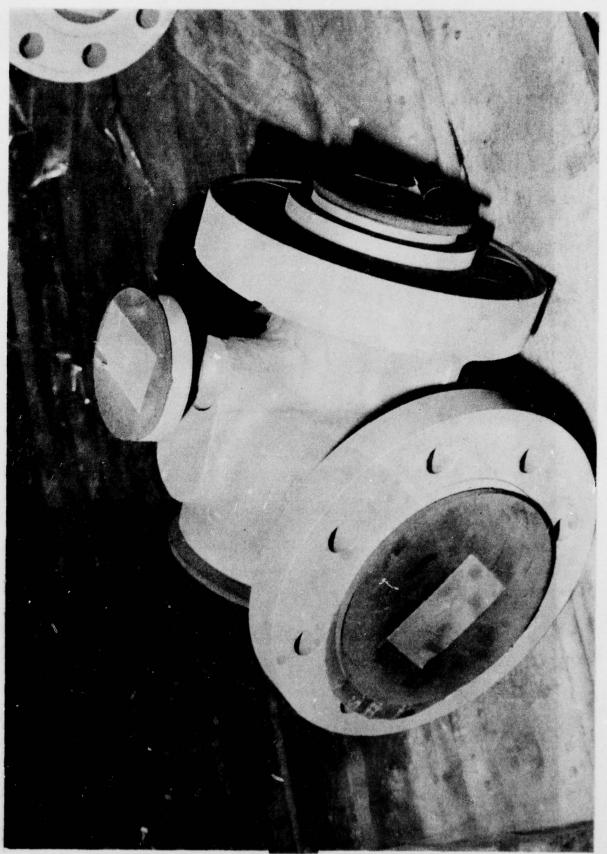


FIG 36

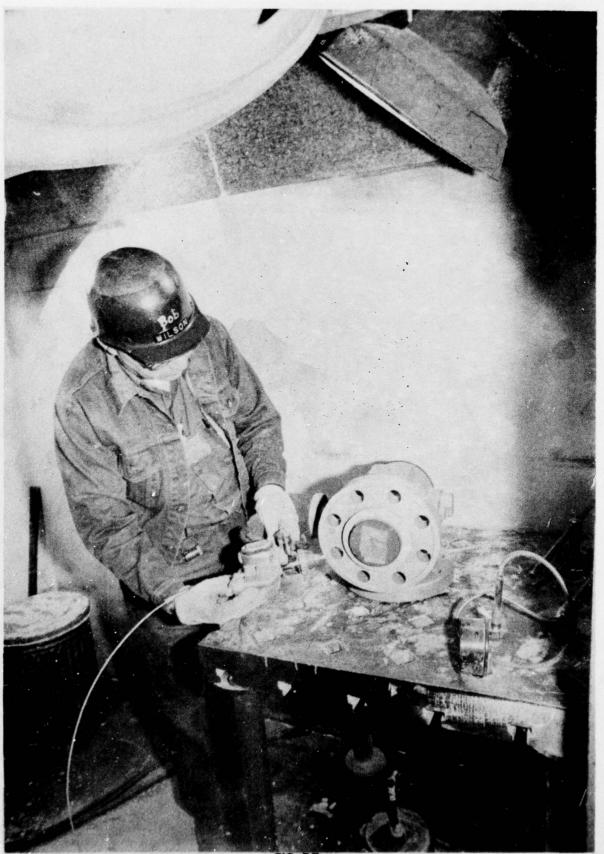


FIG 37

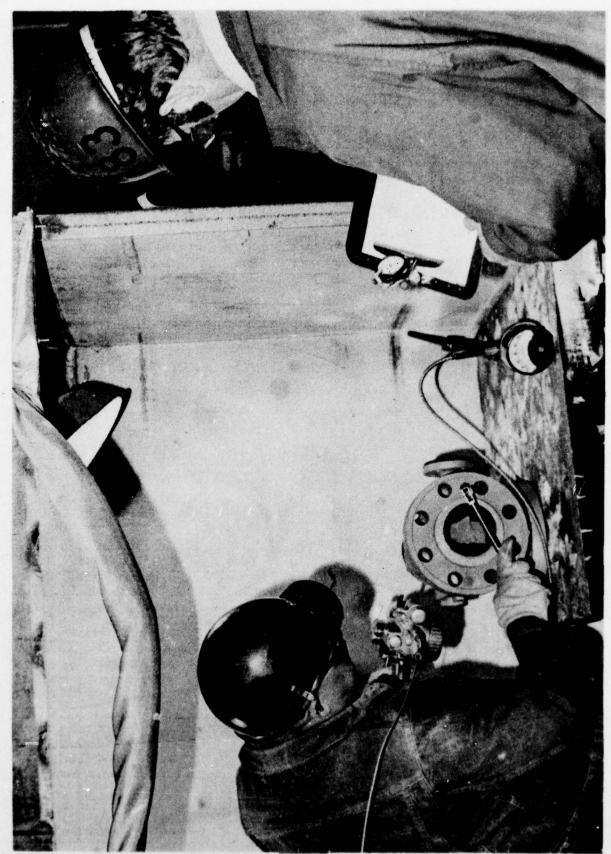


FIG 38

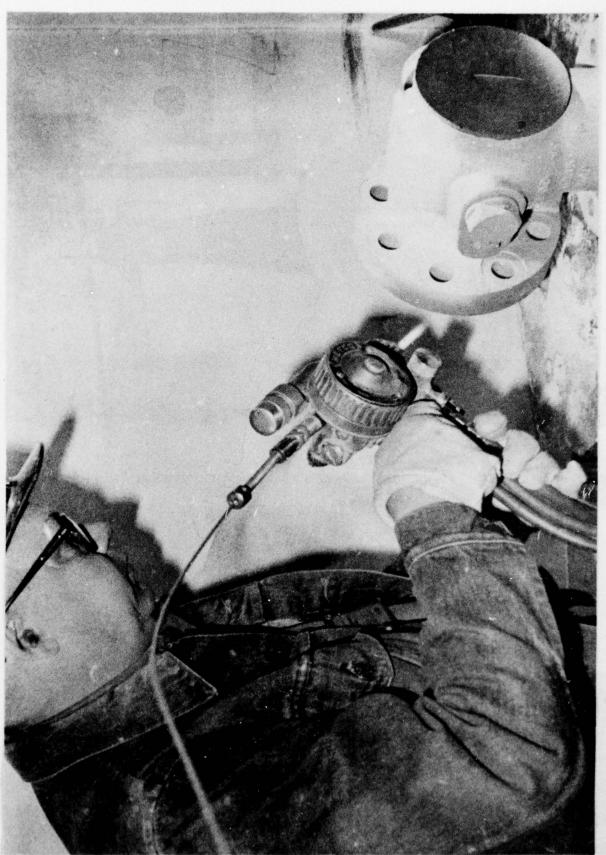


FIG 39

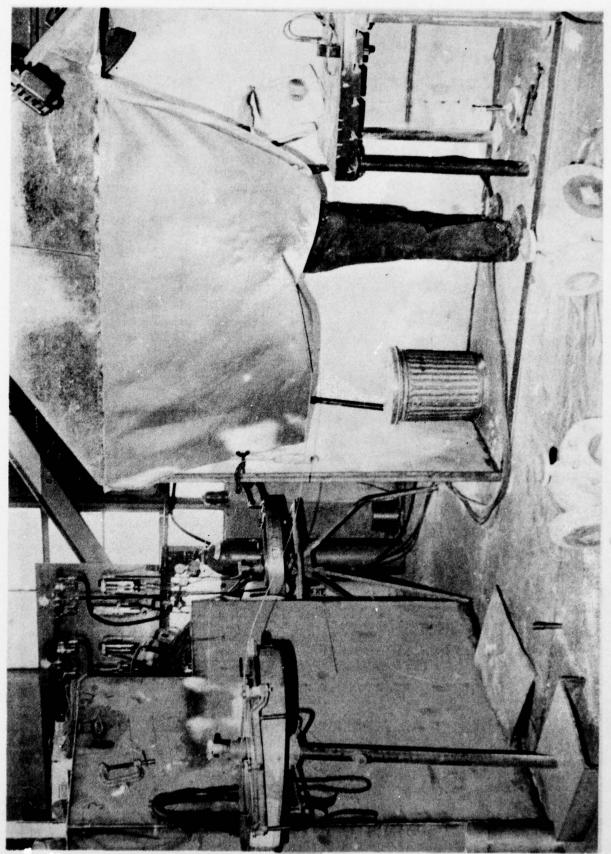
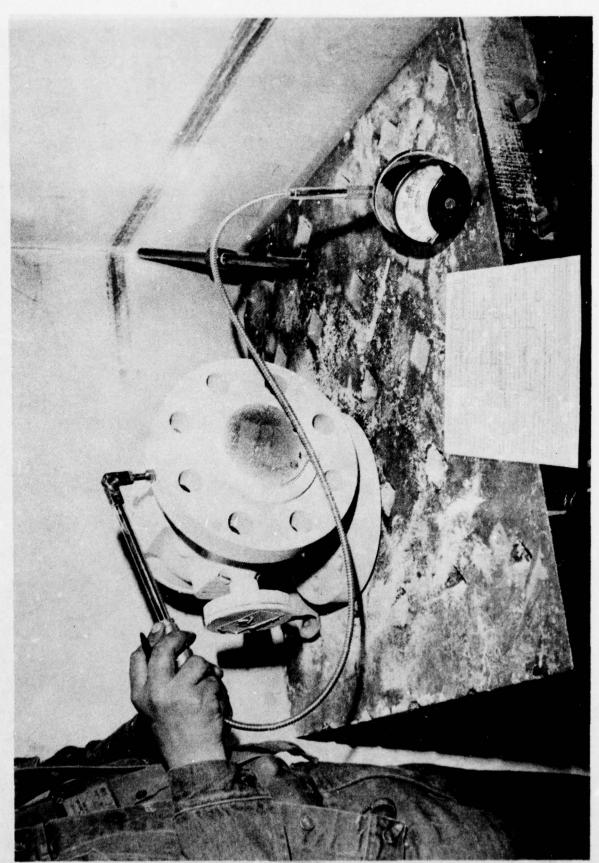


FIG 40



F16 41

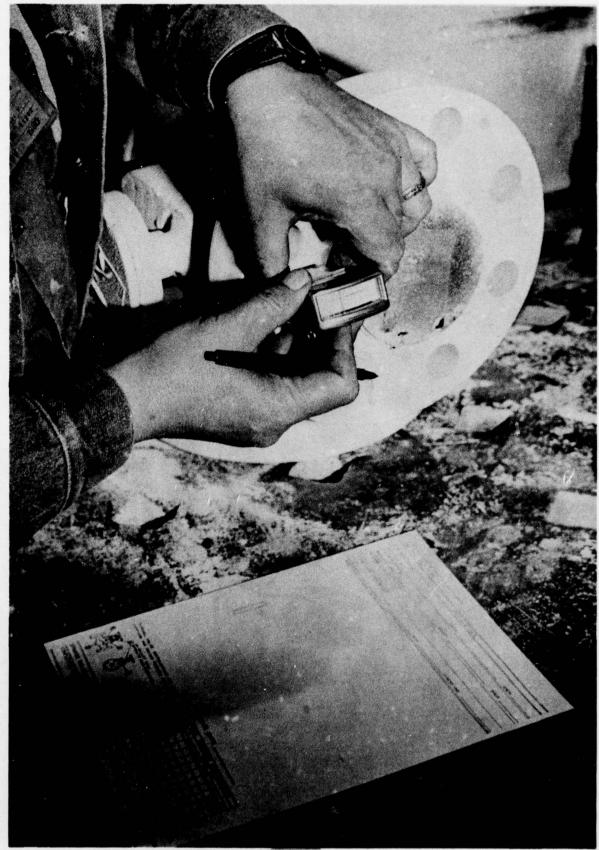


FIG 42



FIG 43

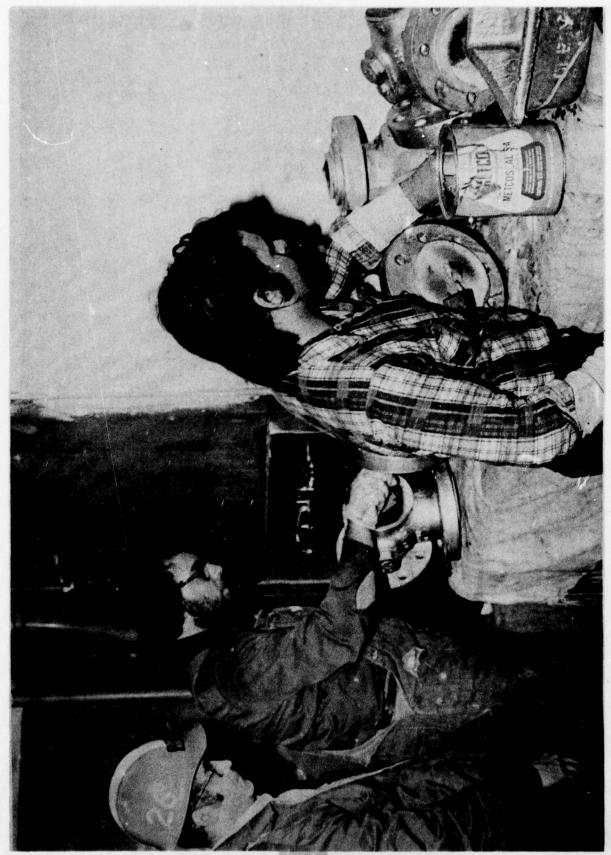


FIG 44

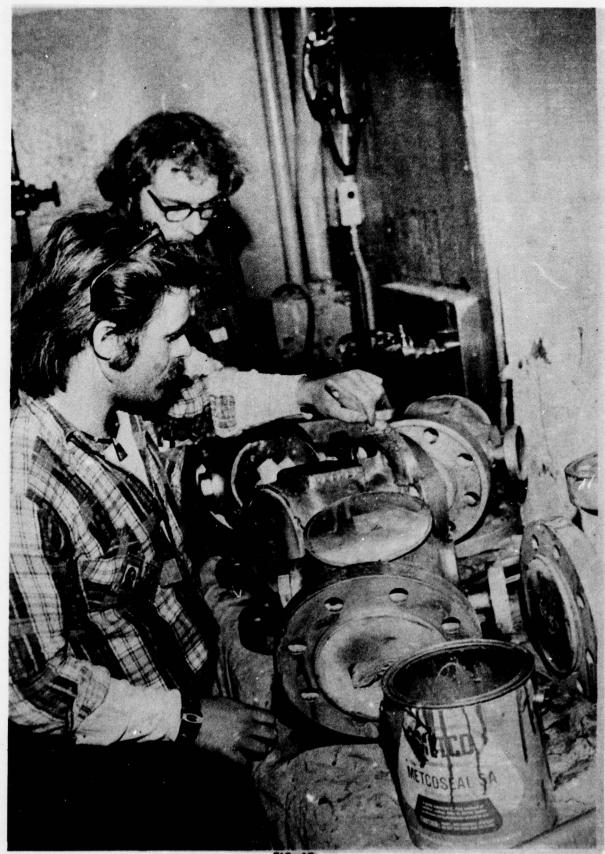


FIG 45

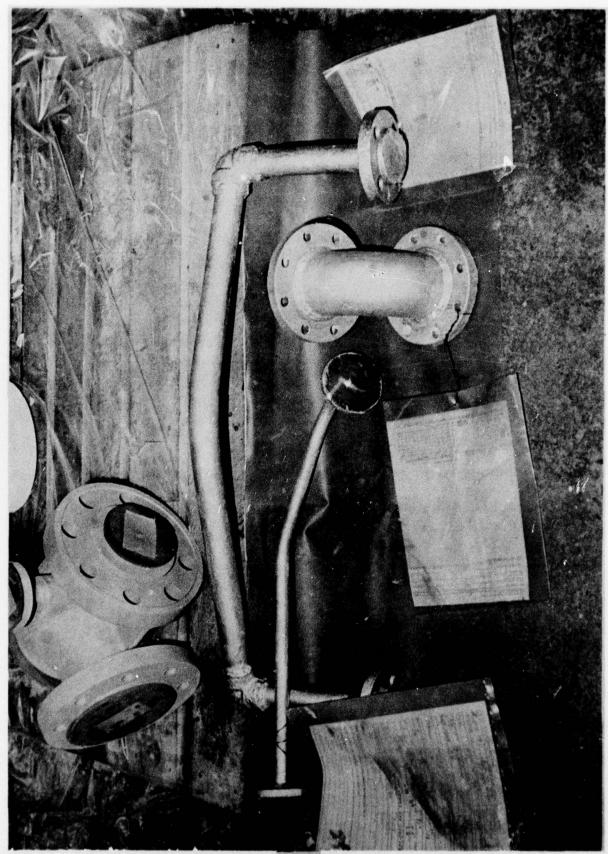


FIG 46





FIG 48

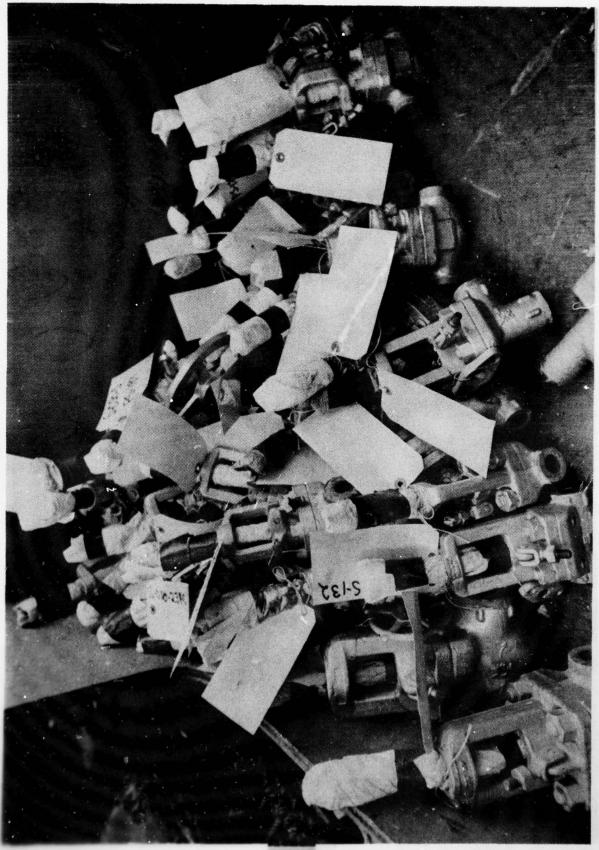


FIG 49

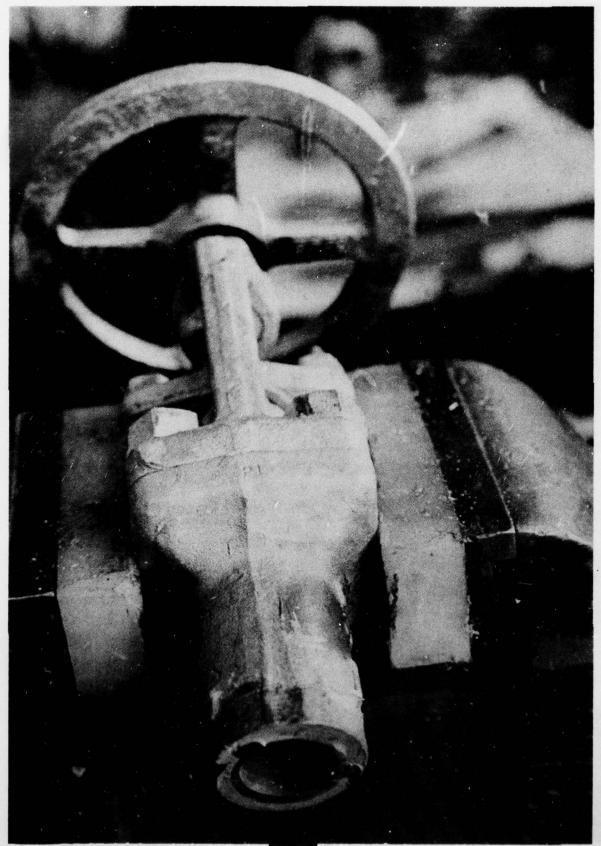


FIG 50

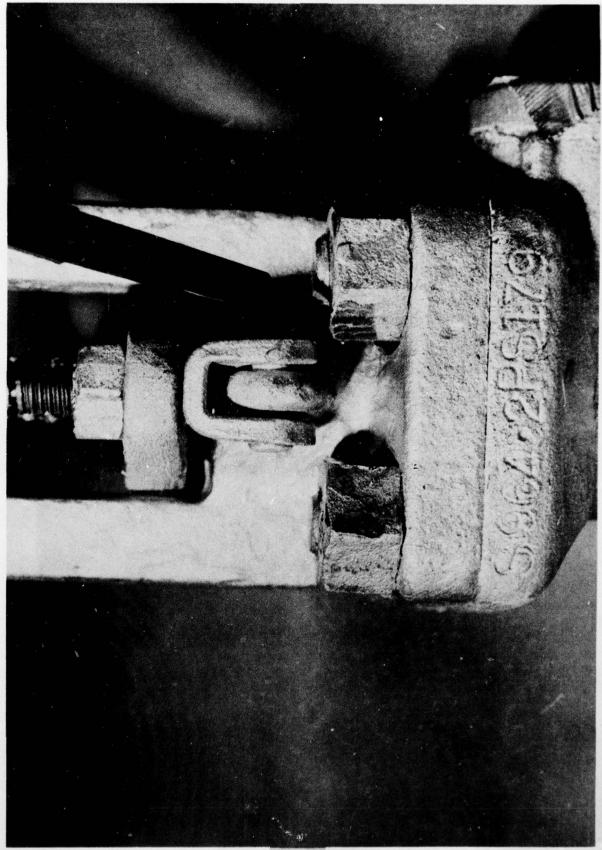


FIG 51

CONTENTS 1 GALLON U.S.

METCOSEAL SA

(SILICONE ALUMINUM

A special material for finish

STOP CORROSION WITH MET

MIX WELL BEFORE USING

1 U.S. LB

AUGUST 76 BATCH 8175 DSA-60076-11-21-00

9150-00-823-7038 BEL.RAY ANTI-SEIZE 70

EXTREME PRESSURE GREASE OFDWANCE

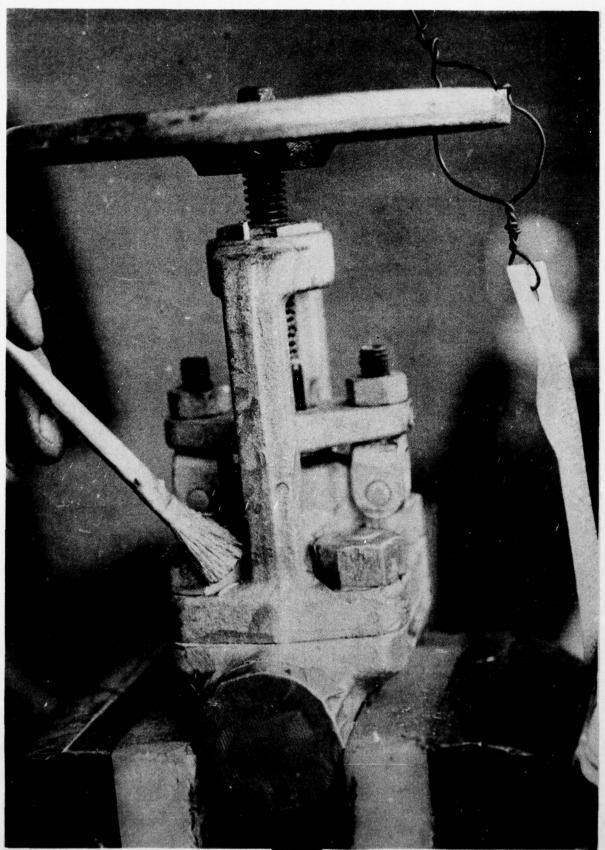


FIG 53

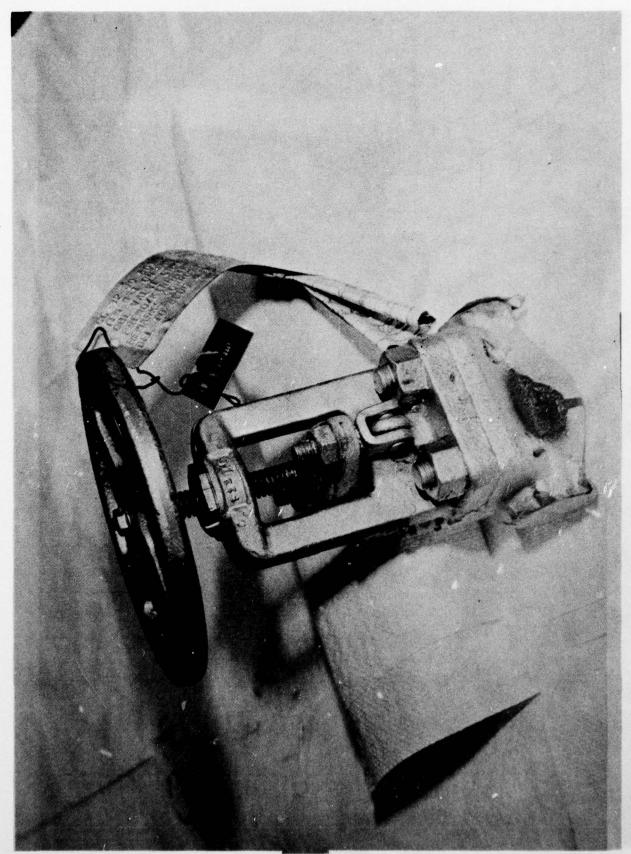


FIG 54

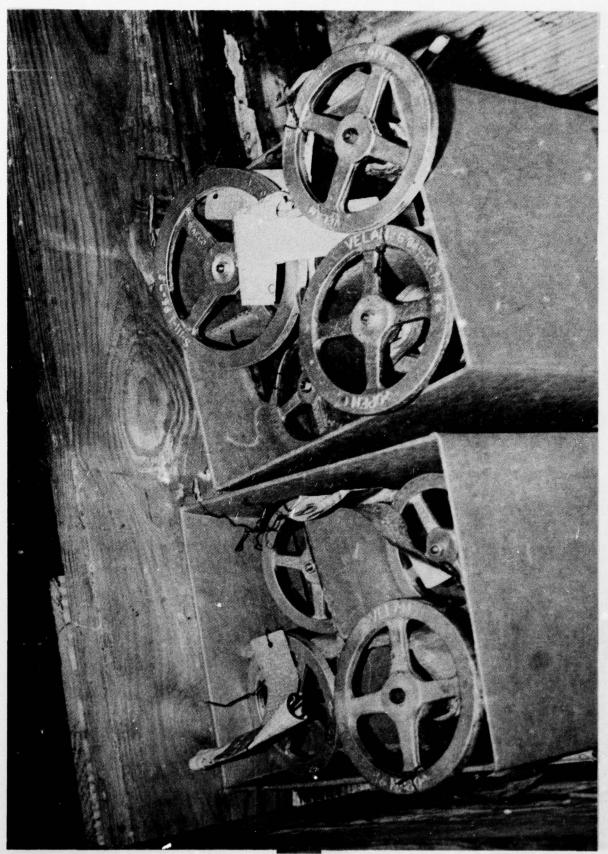


FIG 55



FIG 56

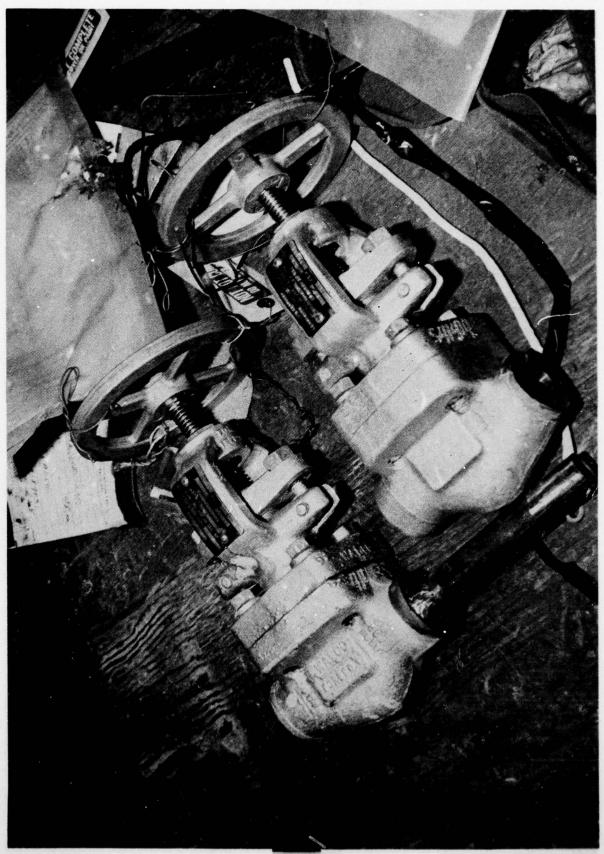


FIG 57

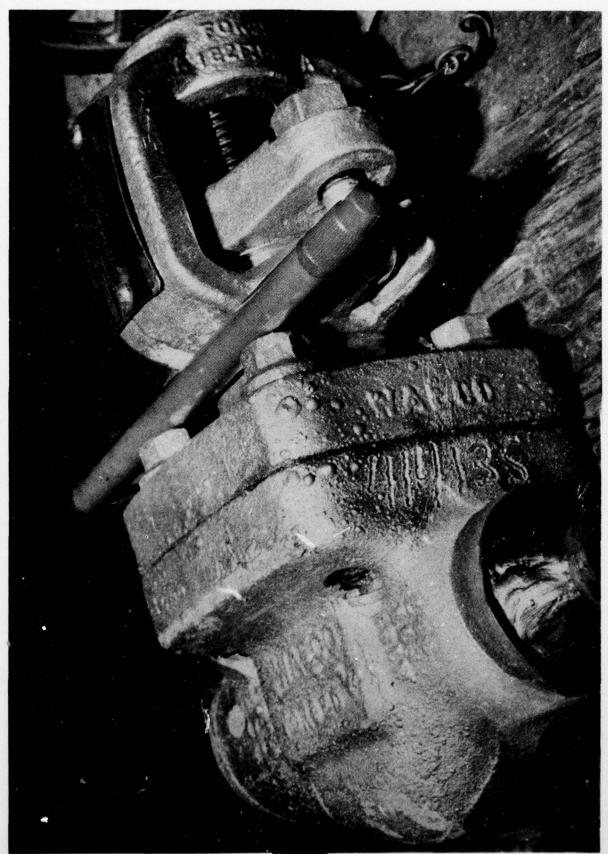


FIG 50

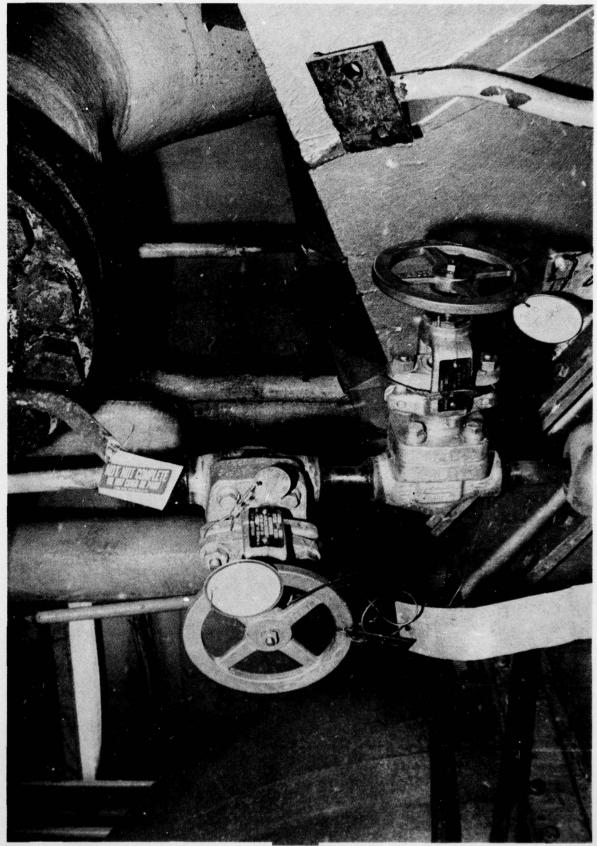


FIG 59

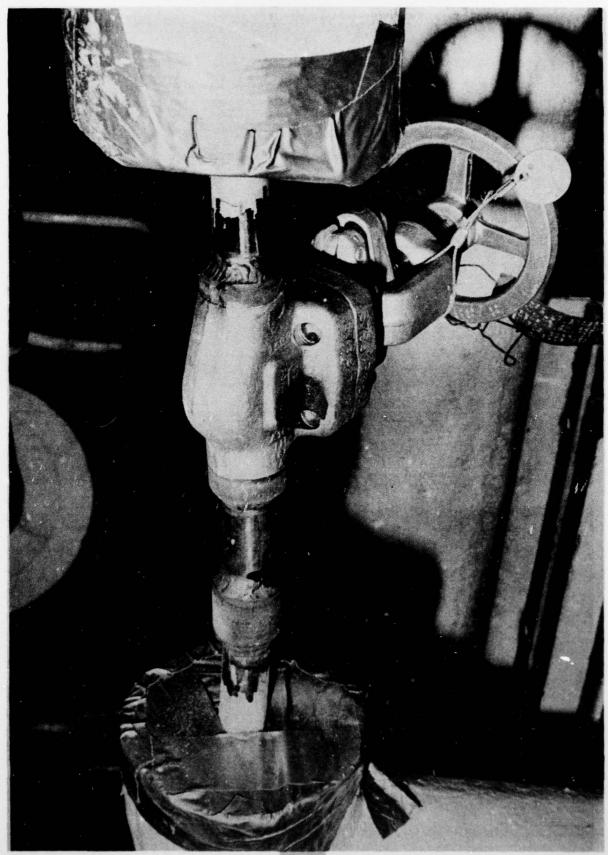


FIG 60

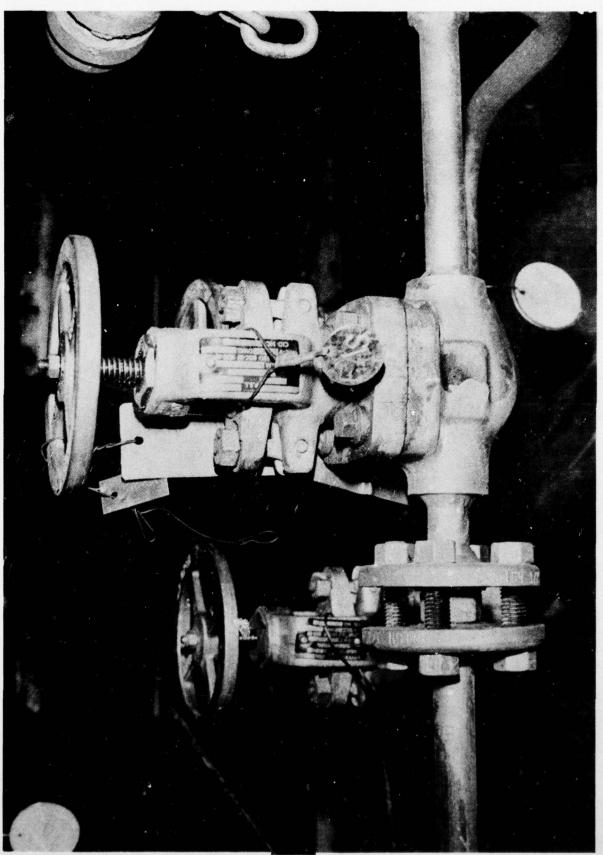


FIG 61

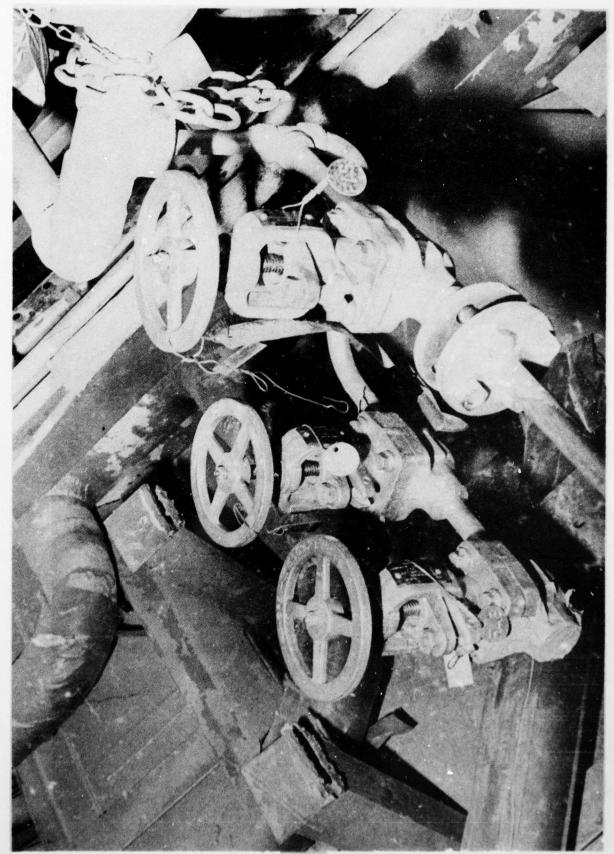


FIG 62

AD-A062 704

PUGET SOUND NAVAL SHIPYARD BREMERTON WASH
ALUMINUM WIRE SPRAY METALLIZING SHIPBOARD COMPONENTS FOR CORROS--ETC(U)
JUL 78 W H STANDLEY, M D SCHMELLER
PSNS-WER-0161
NL

UNCLASSIFIED



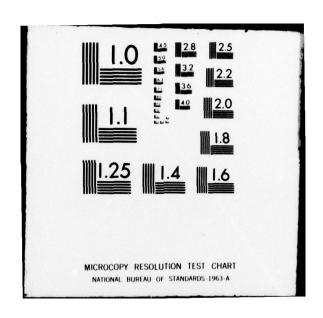








END DATE FILMED



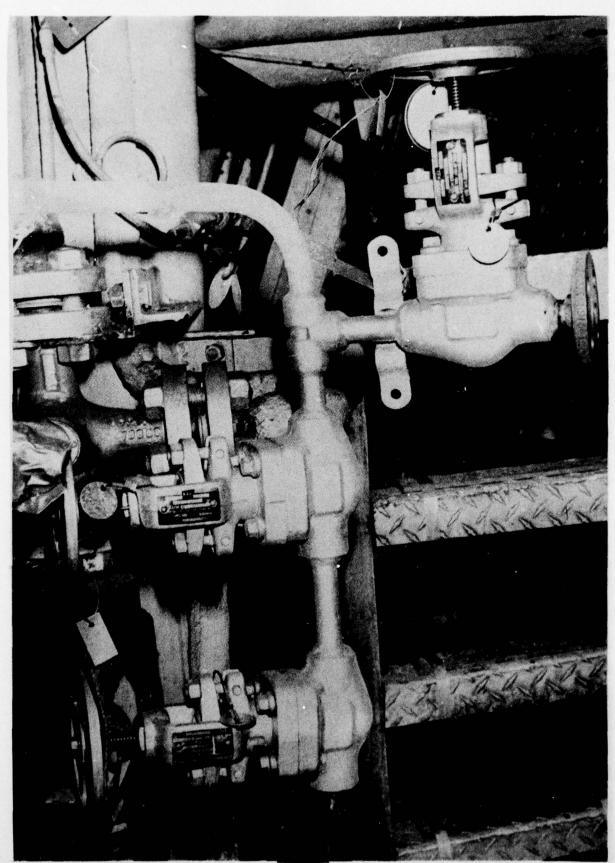


FIG 68

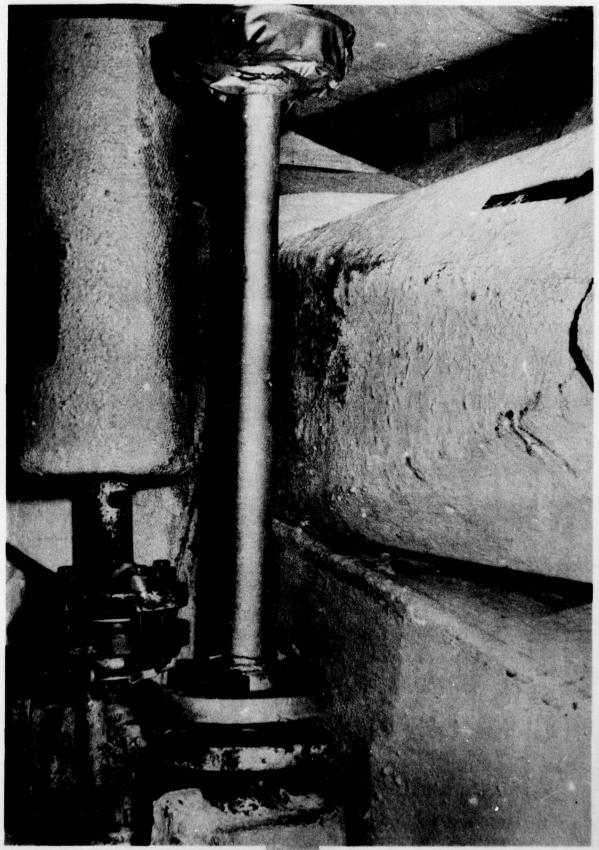
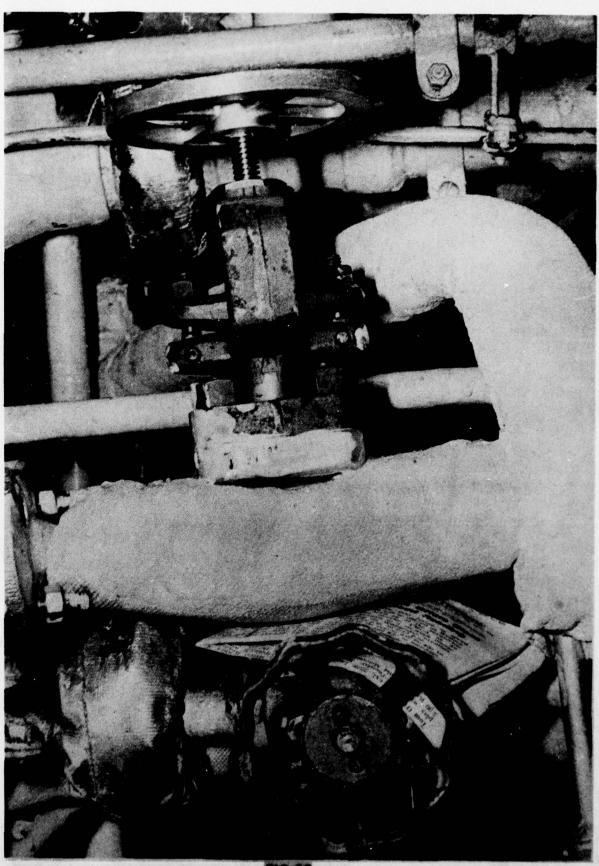


FIG 64



FIG 65



P10 88